

# Compact Instrument for Stray-light Detection and Diagnosis in Telescopes

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**Author / Presenter:**

Dr. William P. Kuhn  
Opt-E  
3450 S. Broadmont Dr., Ste. 112  
Tucson, AZ 85713  
[bill.kuhn@opt-e.com](mailto:bill.kuhn@opt-e.com)  
520-867-8632 (o)      520-907-3988 (m)

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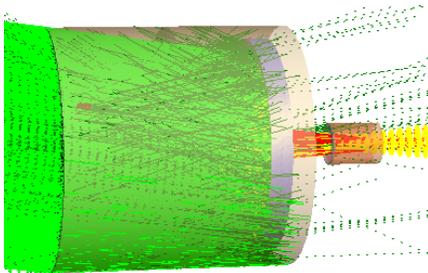
# Acknowledgements

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  - Mr. Rich Pfisterer – Photon Engineering
  - Mr. Steve Mulder – Photon Engineering
  - Mr. Armand Sperduti – Intaq
  - Mr. Garry Knight – EE consultant

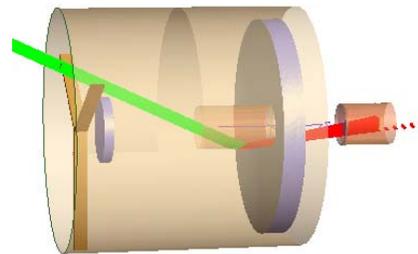
# Stray Light Detection & Diagnosis

## Stray light detection and *diagnosis*

Old way – detection only – yellow/red rays are stray light, Where did they originate?



Full aperture simulation



Subaperture simulation

Diagnose stray light – source of red rays on detector is obvious

## SLDD Uses

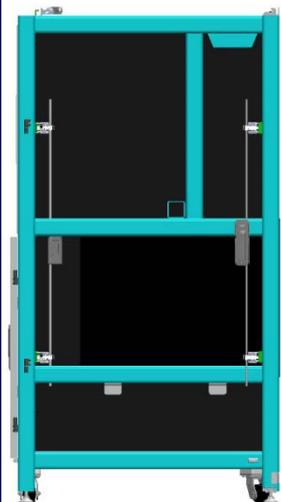
- Sensor design validation before production
- Stray-light model validation
- Thorough evaluation of first article or pre & post stress test
- Modest evaluation of assemblies in production
- Can evaluate: 1) complete sensor, 2) sensor with surrogate detector or 3) detector assembly

## SLDD Capabilities

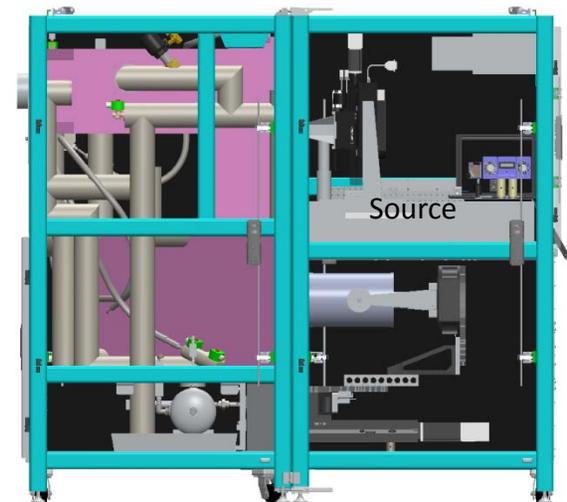
- ~1 min per field point
- Max 10" diameter aperture, 20 deg field, all azimuths
- Purged cabinets and in clean room
- Choice of ambient temperature or cryogenic beam dump
- 2 cabinets have about 35 sq. ft foot print

## Technology: Subaperture illumination for stray light detection and diagnosis (SLDD)

- Old way → illuminate full aperture, analyze, experiment
- SLDD → subaperture illumination provides additional information about defect path → reduce analysis time
- SLDD → increased irradiance at aperture & reduced background → increased sensitivity & smaller instrument
- Trade-off in use between scanning speed and sensitivity
- 640 nm, 60 mW laser with speckle reduction
- 8.56 μm, 750 mW laser, Fabry-Perot QCL (broad spectrum)
- Easily configured to other wavelengths
- Contamination dominates instrument signature – small optics are used – CO<sub>2</sub> snow clean and replace as needed



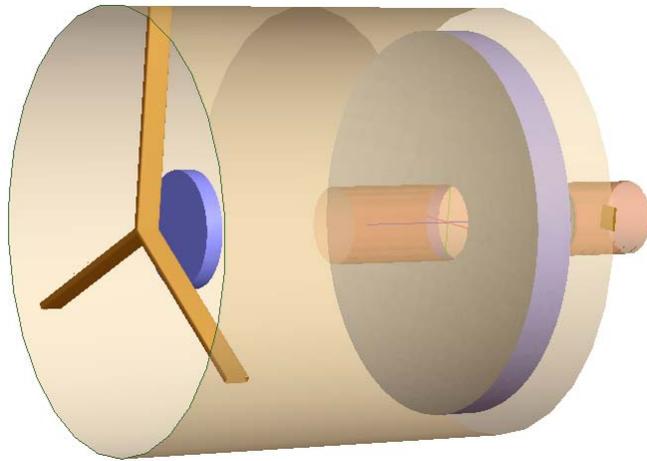
Ambient beam dump



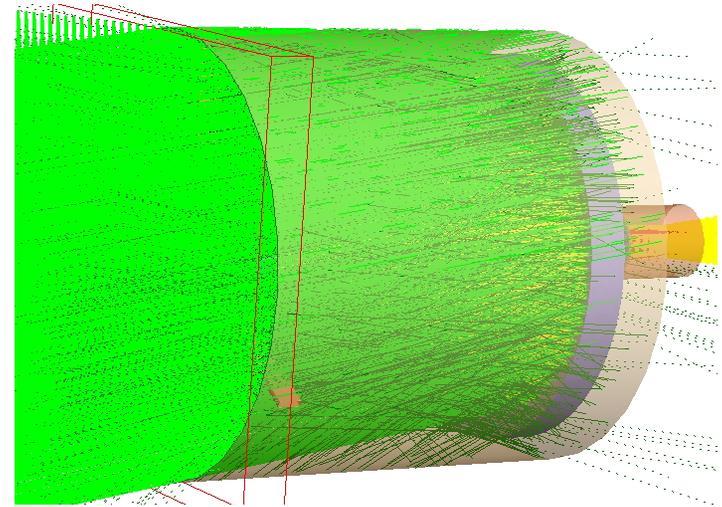
Cryo beam dump UUT (Celestron C8)

## Simulation – full aperture

- Cassegrain telescope modeled using FRED™ software from Photon Engineering
- Right image – green lines are incoming rays from a source outside the FOV. The yellow rays on the right are outgoing stray light that made it to the detector.
- What caused the problem?
  - Easy to determine in simulation for the program tells you the ray paths.
  - In a hardware test, the answer is not necessarily obvious.



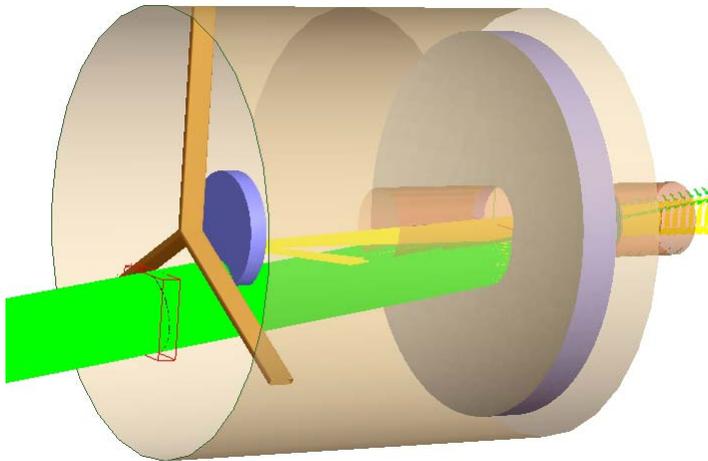
FRED simulation of a Cassegrain telescope



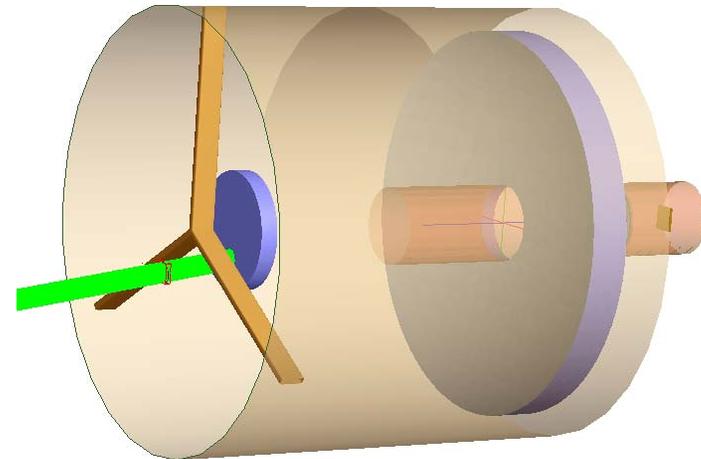
FRED simulation of a Cassegrain telescope with full aperture illumination

## Simulation – subaperture

- A small beam ( $\sim 1/8^{\text{th}}$  aperture diameter) that results in stray light is shown in the left image.
  - Green rays that reach the detector are a sneak path – should be found in any reasonable stray light analysis.
  - Yellow rays are due to scatter at the primary and reflection by the secondary to the detector.
- A further reduction of beam size and scanning over the subaperture within which stray light is detected can further refine knowledge of the stray light location



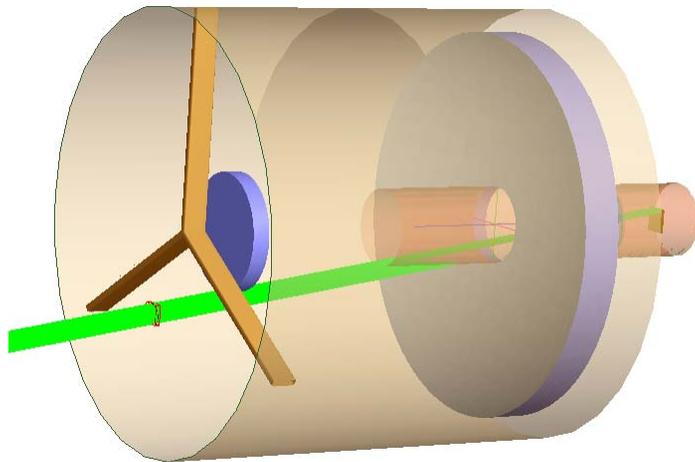
FRED simulation of a Cassegrain telescope with subaperture illumination



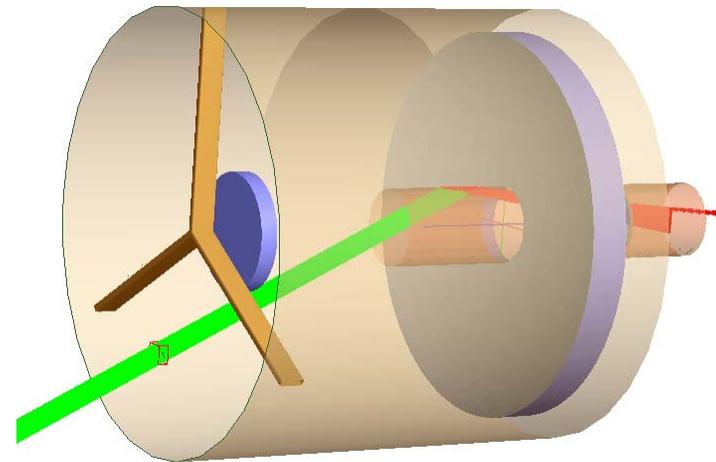
FRED simulation of a Cassegrain telescope with subaperture illumination

## Simulation – subaperture (2)

- Left image – continuation of scan within region where stray light was detected –
  - A sneak path by the secondary has been discovered (green light to detector)
- Right image – beam from a larger off-axis angle illustrates a stray light path including a single scatter off of the interior of the detector baffle (red light to detector)



FRED simulation of a Cassegrain telescope with subaperture illumination

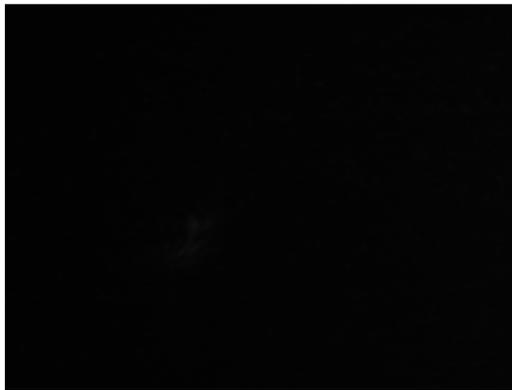


FRED simulation of a Cassegrain telescope with subaperture illumination



## Subaperture concept demo (2)

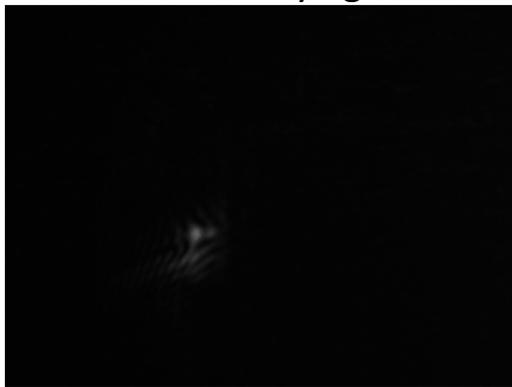
Instead of reducing the beam size and scanning over the subaperture where stray light was detected, a Gaussian beam can be used to encode the position.



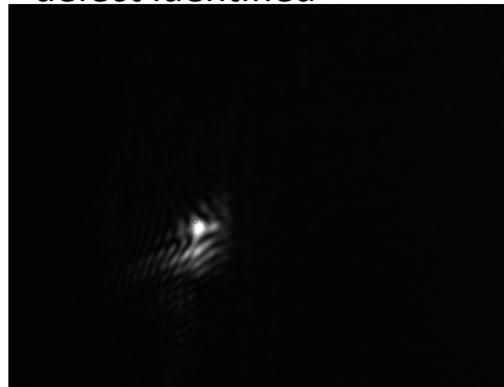
Pos. 1 – no stray light



Lens disassembled – defect identified



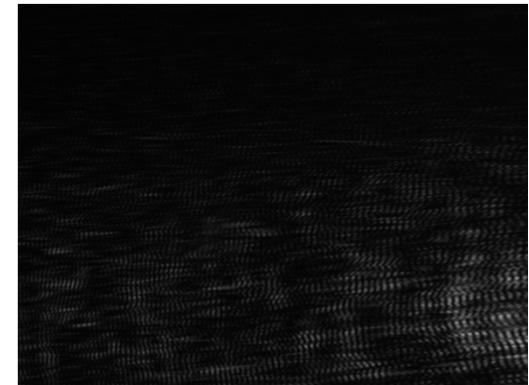
Pos. 2 – stray light



Pos. 3 – stronger signal

Baffle (iris) diameter changed to simulate a different defect type.

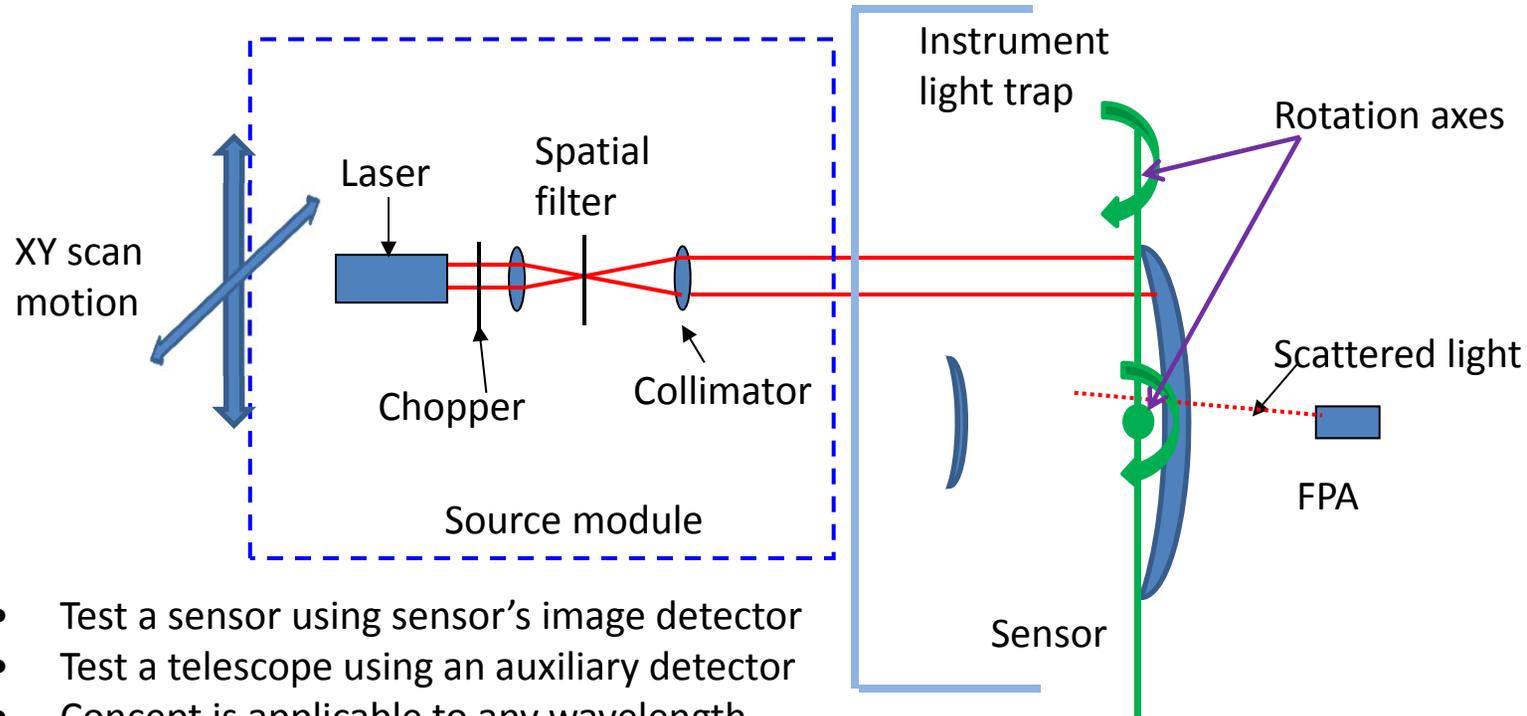
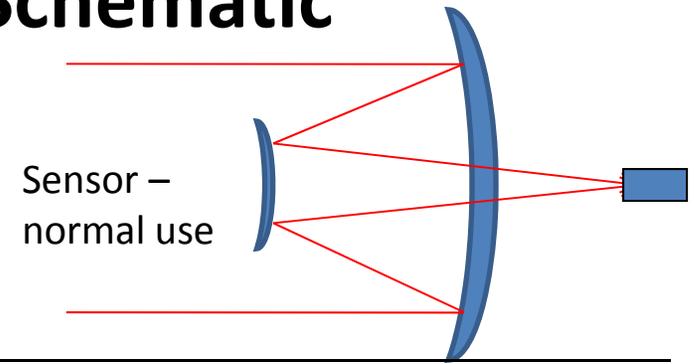
Stray light is present and different than lens defect on left.



Stray light due to scatter from an aperture edge.

# Instrument & Sensor Schematic

- Sensor = telescope + image detector
- 4 motion axes to scan aperture and field
- Source module likely to use reflective, not transmissive optics

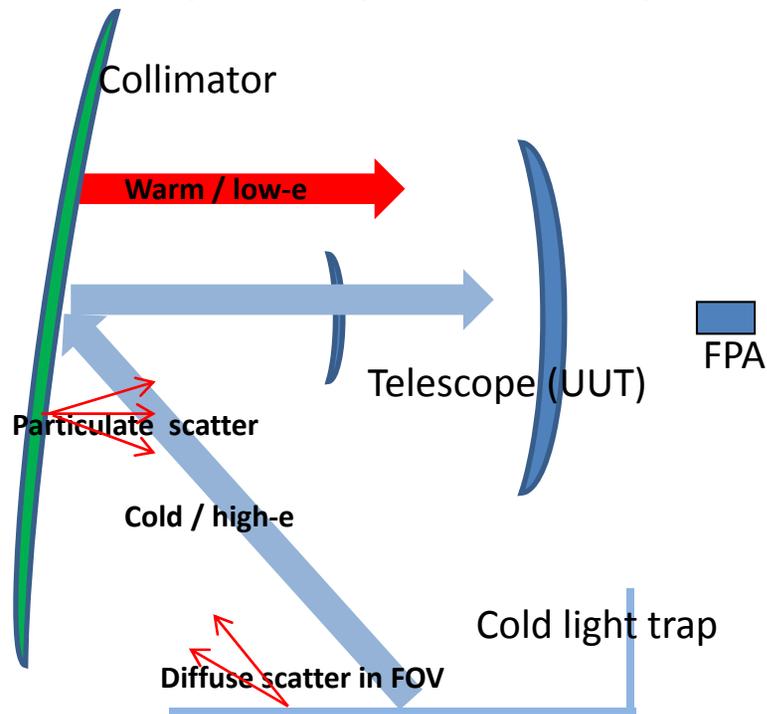


- Test a sensor using sensor's image detector
- Test a telescope using an auxiliary detector
- Concept is applicable to any wavelength
- One possible set of motion axes is shown

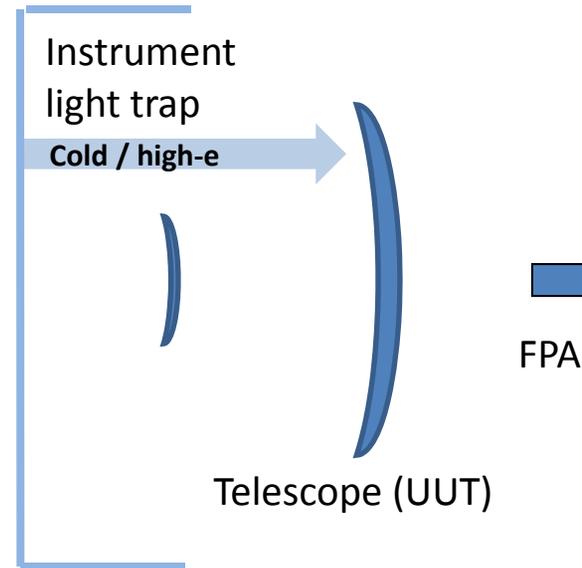
# Cryogenic background comparison

## Full aperture illumination (Breault SLTS<sup>1</sup>)

- Sensor background is combination of:
  - collimator emission – room temperature, low emissivity, and
  - light trap – cold with high emissivity.
- Source power is spread over full aperture.



1. Gary L. Peterson, "Stray light test station for measuring point source transmission and thermal background of visible and infrared sensors", Proc. SPIE 7069, 70690M (2008).



## Subaperture illumination

- Sensor background is from light trap emission – cold with high emissivity.
- Source power is concentrated in subaperture.

## Radiance, 8 $\mu\text{m}$ – 12 $\mu\text{m}$

- Collimator at 295 K and  $e = 0.03 \rightarrow 1 \text{ Wm}^{-2}\text{sr}^{-1}$
  - Light trap at 100 K and  $e = 1 \rightarrow 0.004 \text{ Wm}^{-2}\text{sr}^{-1}$
- $\sim 250\text{x}$  reduction in background at image detector  
([www.SpectralCalc.com](http://www.SpectralCalc.com))

# Source selection

- Need a bright source to simulate sun within wavelength band of interest.
- Bright source implies a laser, but desire short coherence so as to avoid speckle in stray light measurement.
- Visible source:
  - Does not need to consider background emission.
  - Many cameras, and even photodiodes, can be used as surrogate detectors and are available with modest to low-noise at moderate cost.
  - Speckle reduction feature of Toptica iBeam Smart PT laser is desirable.
  - Nominal 640 nm source selected since wavelength is long enough to use with gold mirrors
- LWIR source:
  - Power density higher than sun can be used to compensate in part for background emission.
  - A 295K beam dump emits about 9000x the power as a 100K beam dump in the 8-12  $\mu\text{m}$  band.
  - Aries QCL laser (8.6  $\mu\text{m}$  wavelength) provides easy power level control and operates on air cooling.
  - Fabry-Perot laser cavity provides relatively broad spectrum resulting in modest coherence source.
  - High power ( $\geq 750$  mW) QCL laser and  $\sim 1000$ x sun brightness almost compensates for use of room temperature background with a desensitized camera and provides good S/N for stray light detection with a microbolometer camera.
  - Broad power range and attenuators can allow for safe low power operation on initial scans.

# Source irradiance

- The sun is the primary stray light source. Approximate it as a 6000K black-body with a 0.5 degree (2θ) diameter. Ignoring the effect of the atmosphere, what is the irradiance on the telescope (unit) under test (UUT)? Consider two wavelength bands : LWIR (8-12 μm) and visible (Vis) (0.4-1 μm).

$\Phi = LA\Omega$ , flux = radiance \* area \* solid angle

$\Omega = 4\pi \sin^2(\theta/2) \approx \pi\theta^2$ , θ small and in radians (solid angle of a cone with half-angle θ)

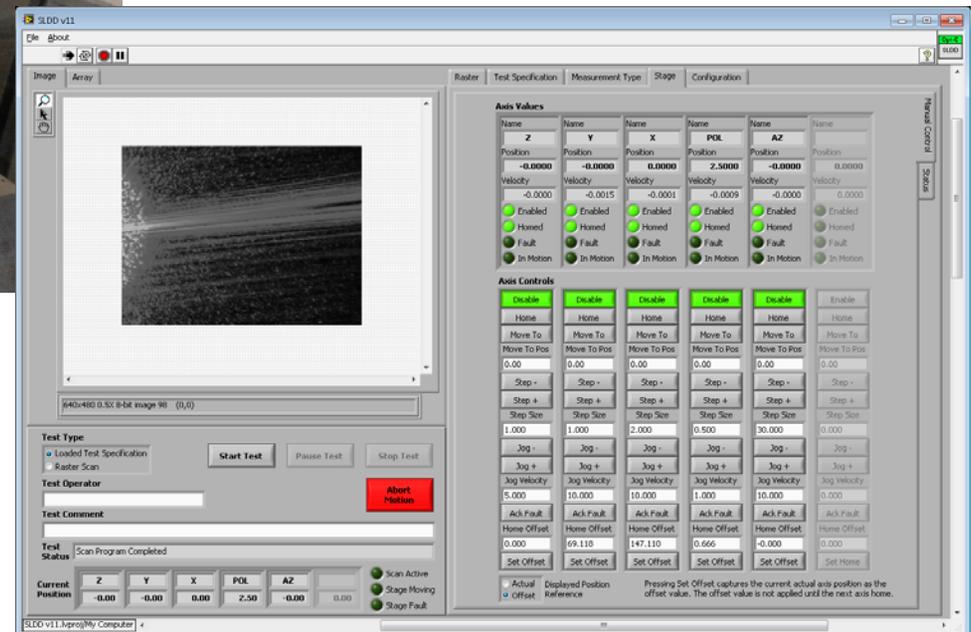
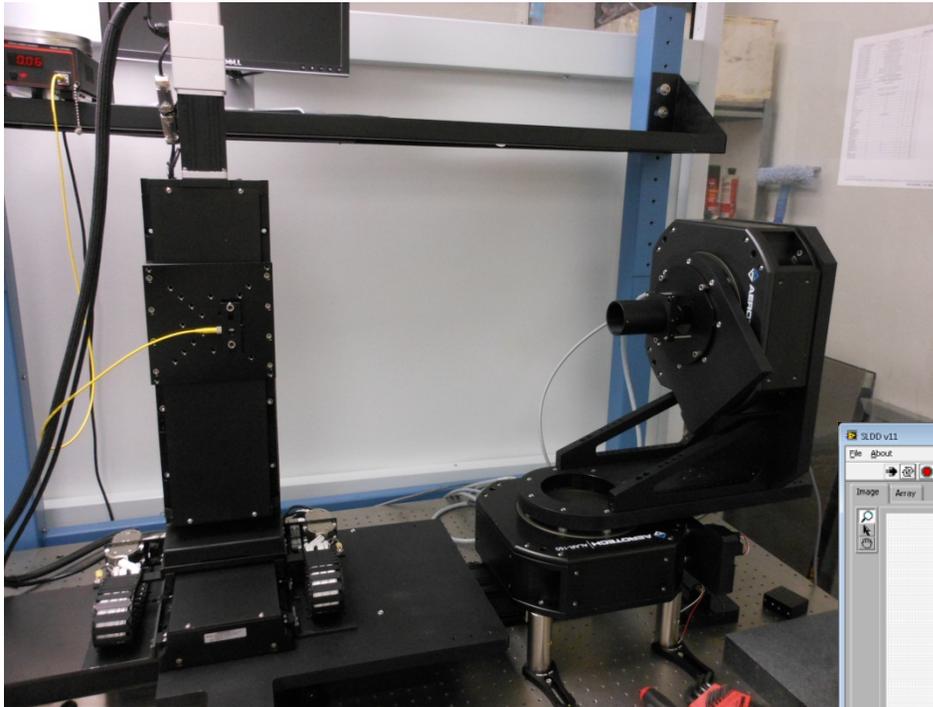
$E = \Phi/A = L\Omega$ , irradiance (Wm<sup>-2</sup>)

Band	Wavelength μm	L Wm <sup>-2</sup> sr <sup>-1</sup>	Ω (sun) Sr	E <sub>sun</sub> mWcm <sup>-2</sup>	E <sub>SLDD</sub> mWcm <sup>-2</sup>	E <sub>SLDD</sub> /E <sub>sun</sub> # suns
Visible	0.4 – 1	1.4E7	6E-5	84	9.5	0.11
LWIR	8 – 12	20000	6E-5	0.12	119	992

E<sub>sun</sub> calculated using [www.spectralcalc.com](http://www.spectralcalc.com) black-body calculator.

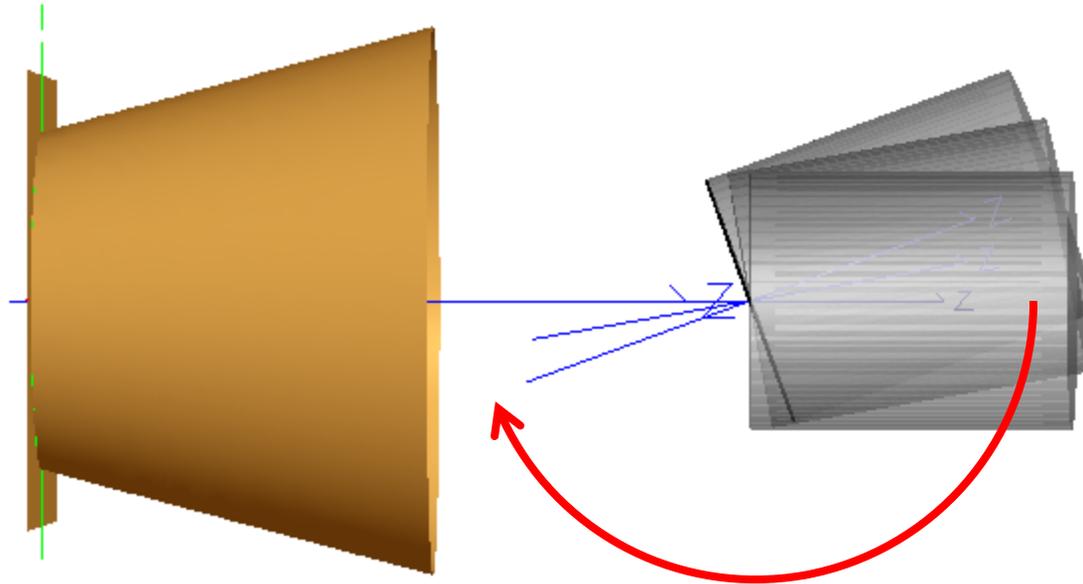
E<sub>SLDD</sub> based on 60 mW visible source and 750 mW LWIR source, T = 50% and 2 cm diameter beam. The Gaussian nature of the beams is ignored in the calculations.

## Baseline visible instrument



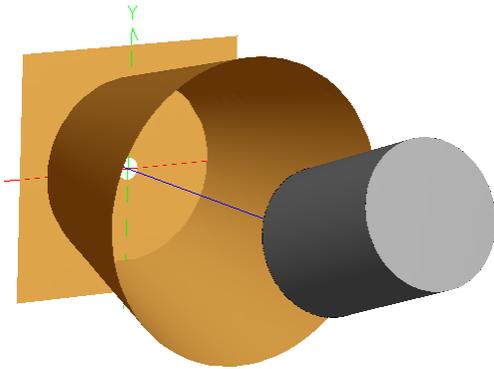
The primary purpose of the baseline instrument is for software development. It will be used with a low power visible source and simple optics. The stages were selected for use in the LWIR instrument.

# Beam dump analysis technique

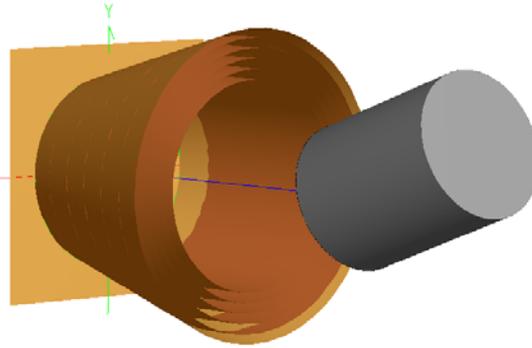


1. System under test is rotated about a fixed point in front of the baffle
2. Rays are traced from the system under test into a  $\pm 2$  deg FOV. The source power is set to unity.
3. Rays are scattered back to the entrance aperture of the system under test
4.  $PST = (\text{scatter power collected on entrance aperture}) / (\text{power emitted by entrance aperture})$

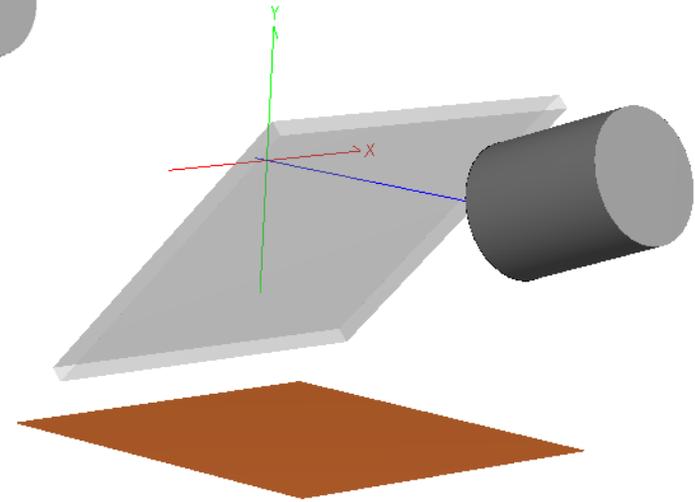
# Beam dump geometries



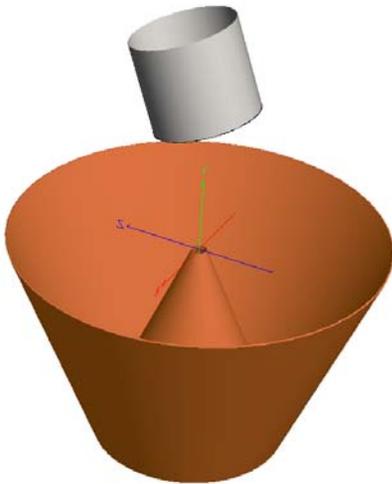
Cone & plate



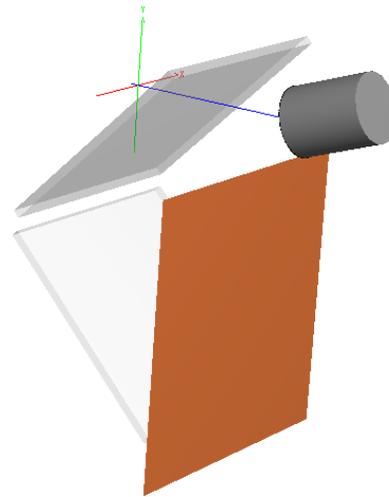
Cone w/ baffles & plate



Single-stage beam dump

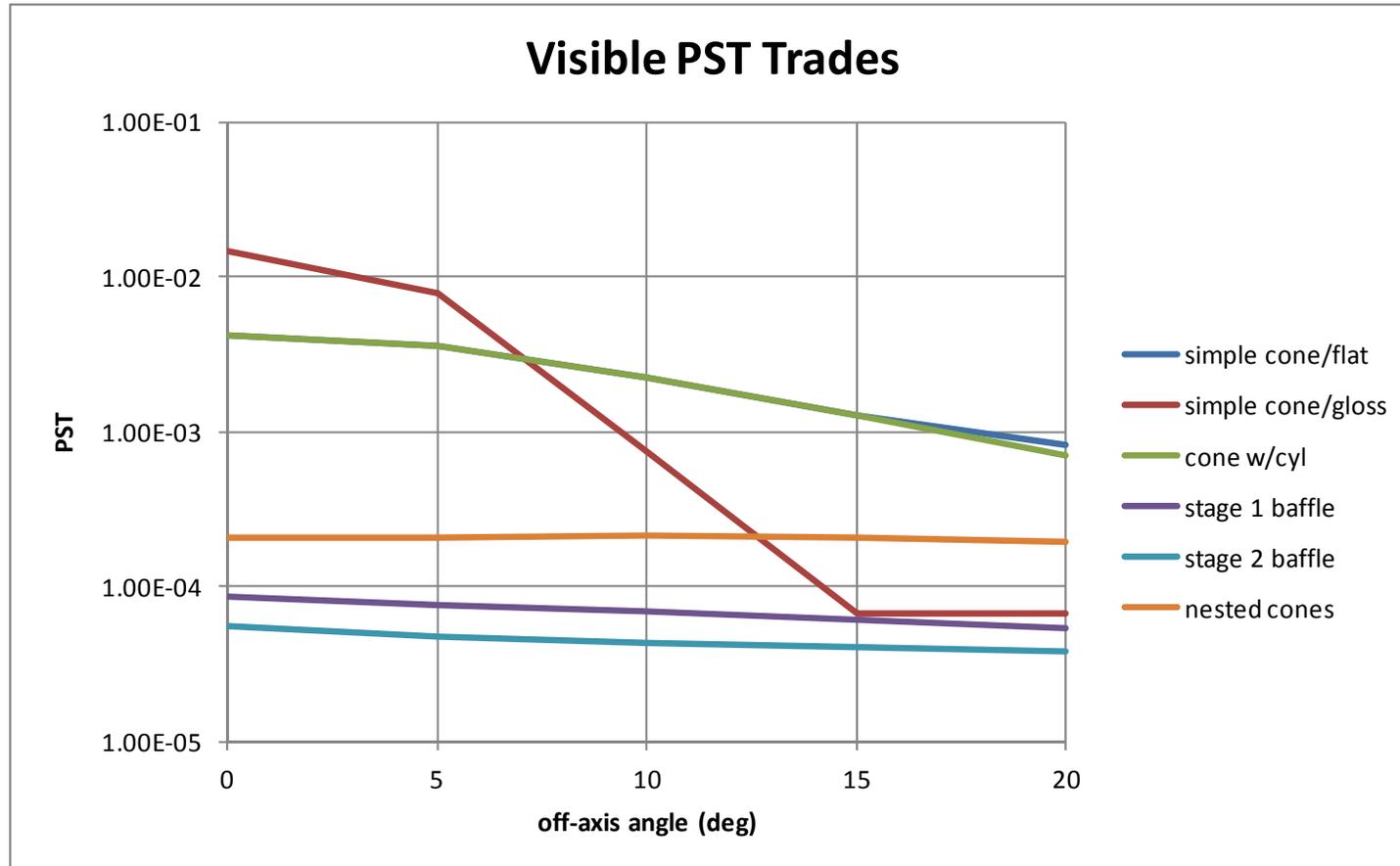


Folded cone

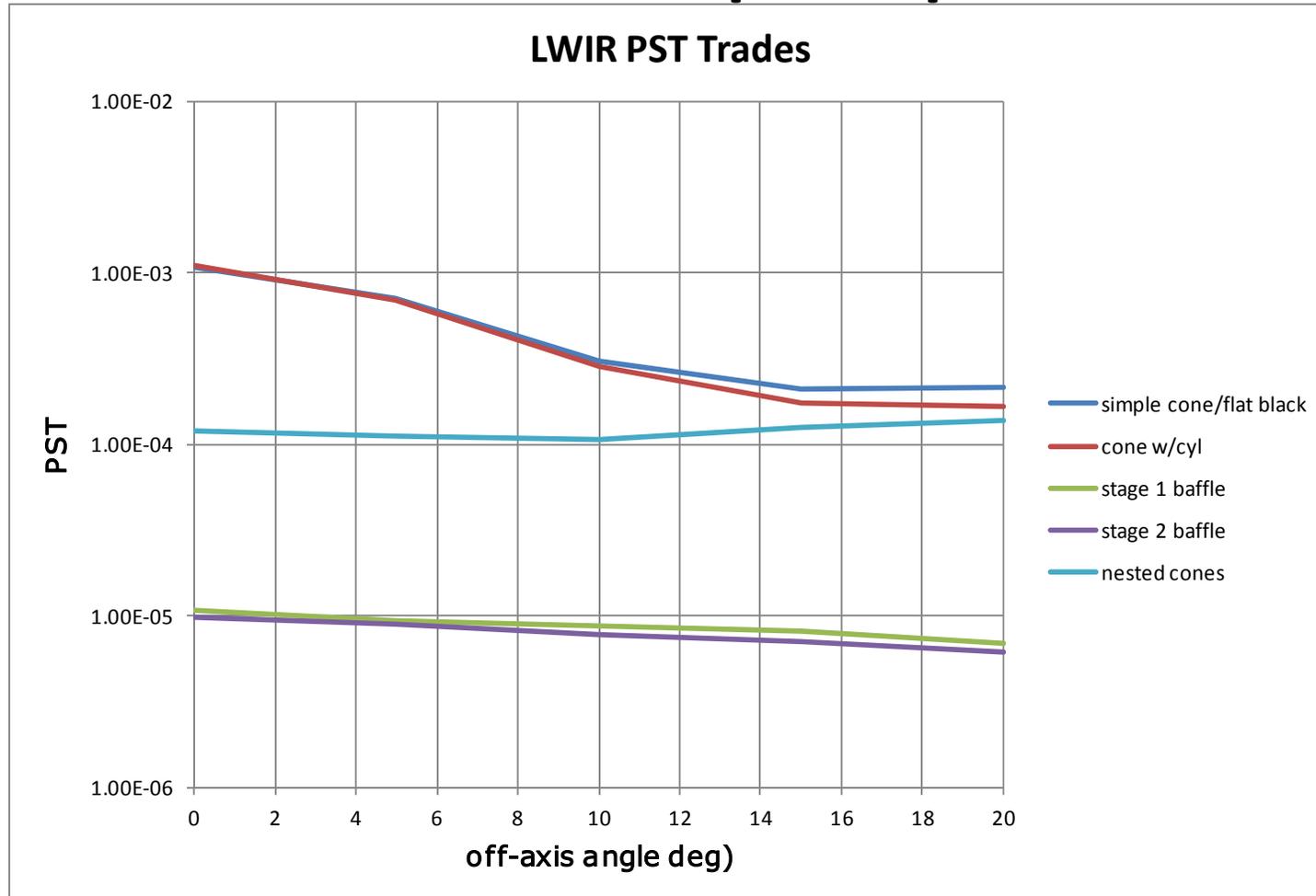


Two-stage beam dump

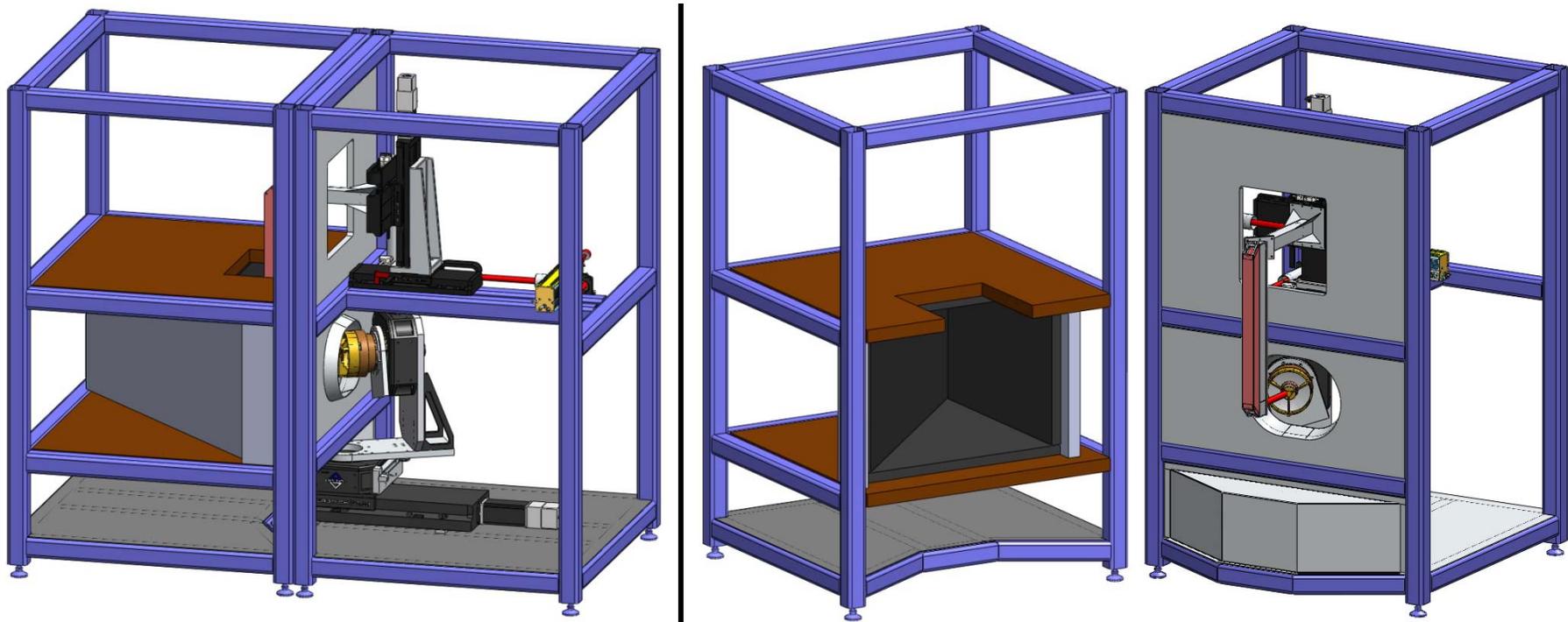
# Visible beam dump comparison



# LWIR beam dump comparison

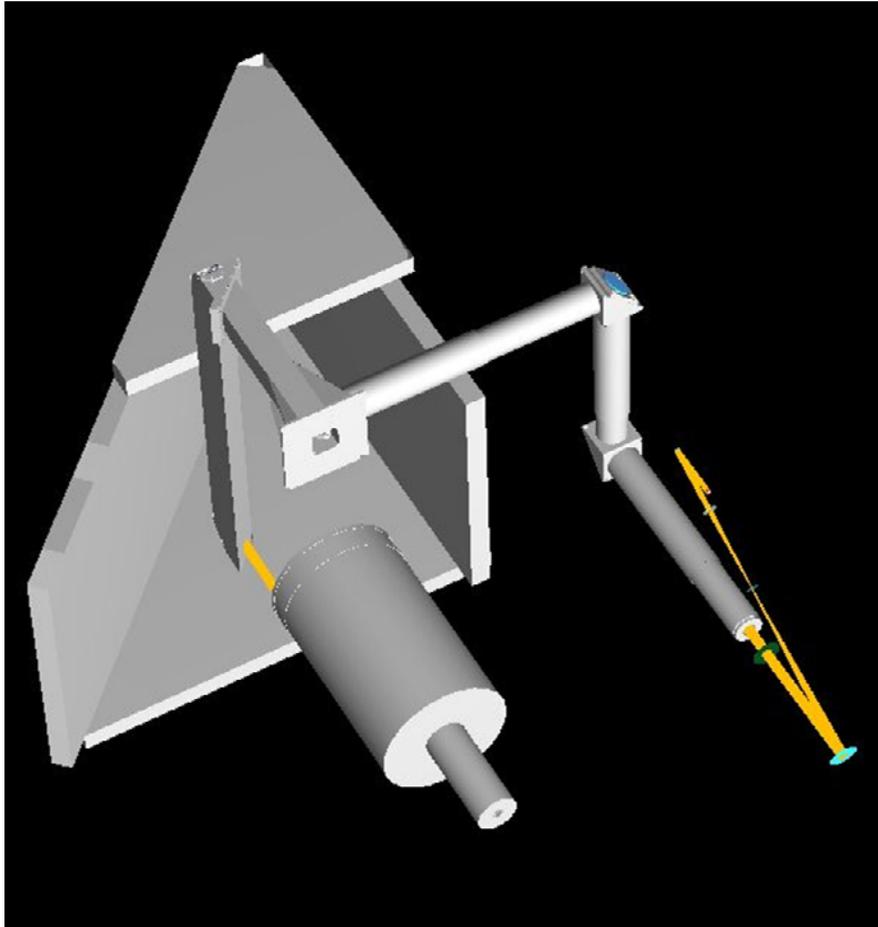


## Simplified SLDD CAD model



Left side shows the two halves of the SLDD instrument together, but with doors and covers removed. The right side shows the instrument opened for service. The cryogenic beam dump is on the left side and is comprised of two rectangular tanks oriented vertically, and two triangular tanks set horizontally. The top tank is hidden. Plumbing, electronics and the source modules are not shown.

## Simplified model in FRED



Basic conclusion is that the instrument signature in the scatter signal of interest is dominated by contamination of the mirrors in the beam delivery system.

The mirrors are 1.5" diameter and 2" diameter flats and replicated OAPs from Newport. They are small enough to CO<sub>2</sub> snow clean and then replace when that is inadequate.

## SLDD Frames



Picture showing 3 frames for SLDD. There is a single source side frame and two beam dump frames. One beam dump is being built with a cryogenic beam dump for use in the LWIR. The second beam dump is for visible light at ambient temperatures.

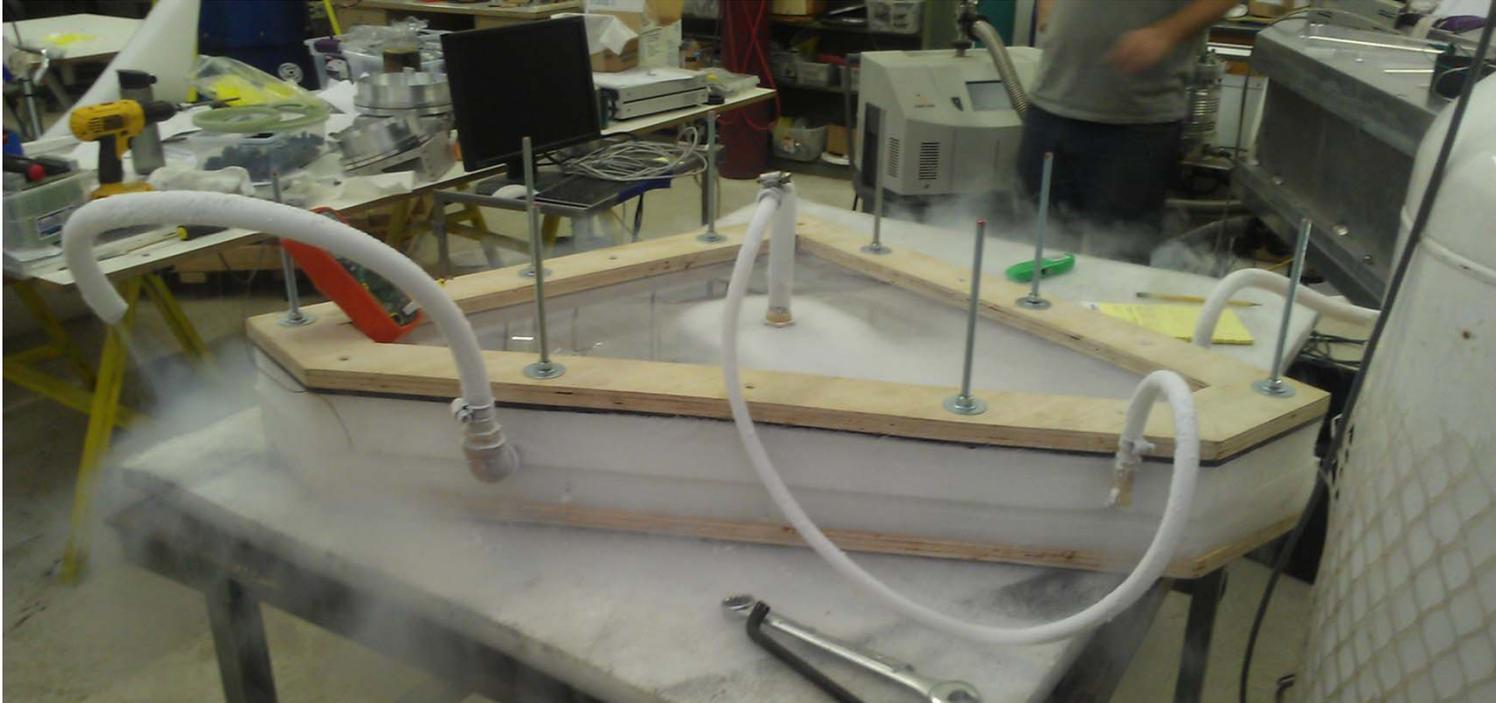
## SLDD Frames

March 11, 2013 – stages / UUT on left, cryo side in clean room on right. Acktar black foil not yet applied to beam dump



March 14, 2013 – behind clean room.

## SLDD Frames



Top tank undergoing cryogenic testing.

# SLDD Instrument



April 26, 2013 – behind clean room.

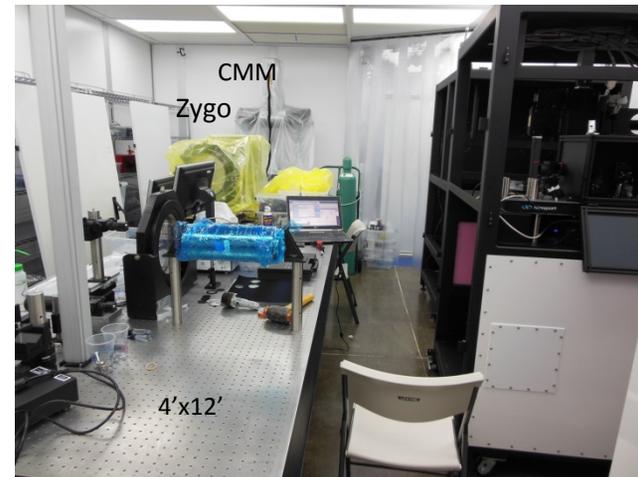
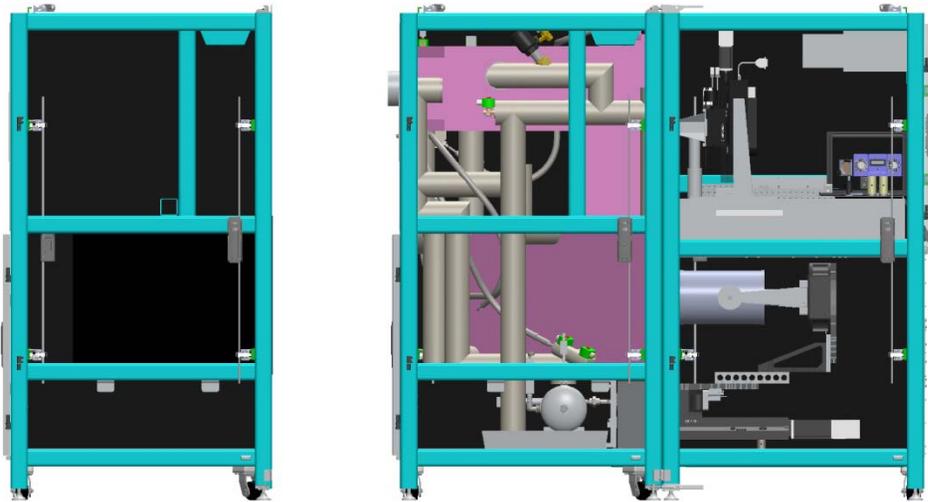


Source platform

April 26, 2013 – stages / UUT side.

### 3 cabinets & room

CAD model of three cabinets on the left and the three cabinets below in the cleanroom.



# Visible light beam dump & Celestron



Visible laser is behind Aries

Aries  
8.6  $\mu\text{m}$

Source bench



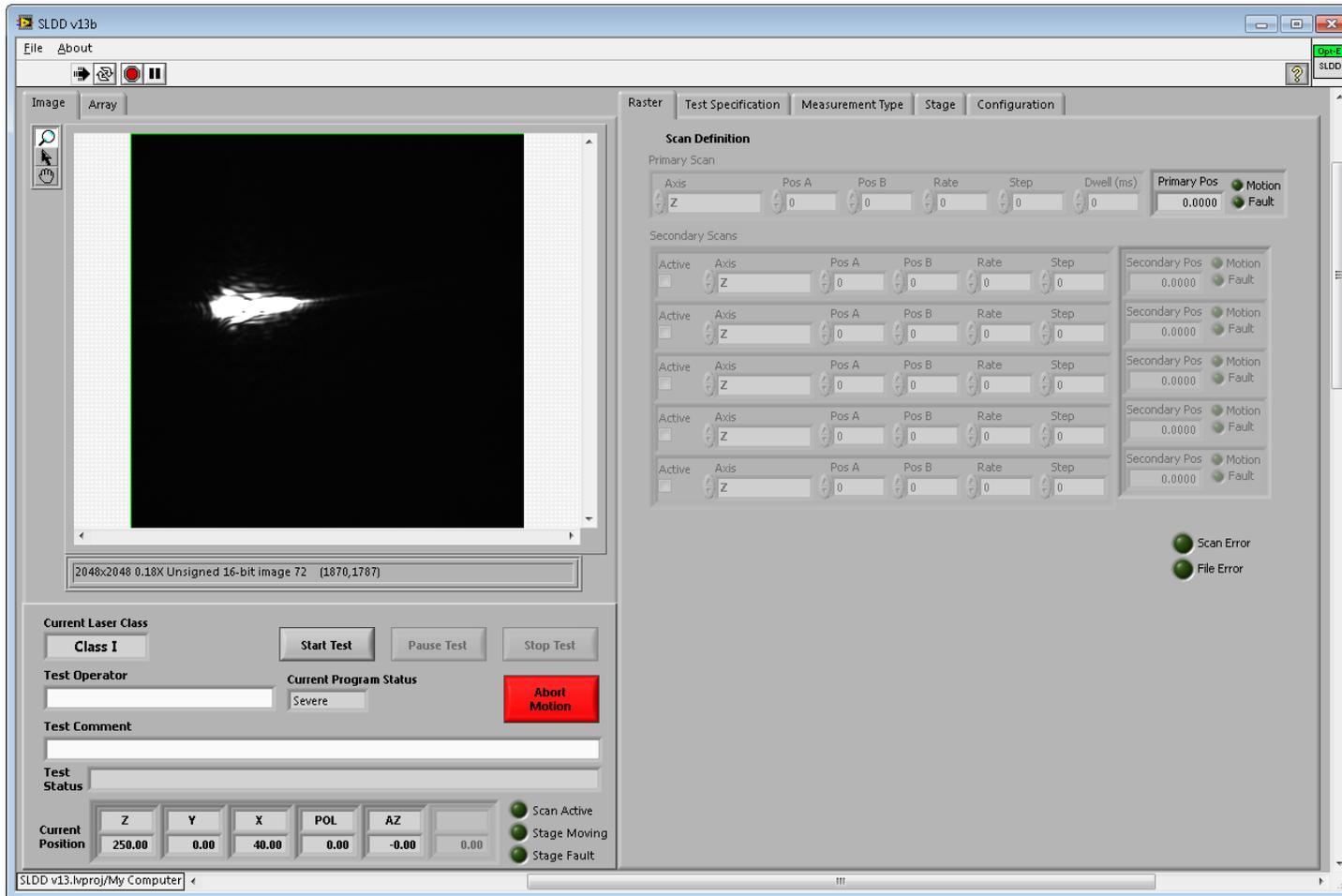
# Cryogenic beam dump



Acktar foil  
(blue wrapping)

# SLDD program – Raster

Live Video



Status

The Raster tab allows for a brute force scan of any combination of axes in any order. Think of it as a set of nested for loops. The motion control is part of the “master program”.

# SLDD program – Test specification

Live Video

Status

The screenshot shows the SLDD v13b software interface. The main window is titled "SLDD v13b" and has a menu bar with "File" and "About". Below the menu bar are icons for navigation and control. The interface is divided into several sections:

- Image Array:** A large window displaying a live video feed of a laser scan, showing a bright spot on a dark background. Below the image, it displays "2048x2048 0.18X Signed 16-bit image 69 (2009,503)".
- Test Specification Tab:** This tab is active and contains:
  - Load Test Spec File:** A button to load a test specification file.
  - Test Information Table:**

Description	Value
Test Name	SLDD Celestron Test 001
Test Creator	Bill Kuhn
Test Comment Scan Program	
UUT Name	Celestron
UUT Model Number	C-8
UUT Serial Number	RichP
  - FOV Table:**

Polar (deg)	Azimuth (deg)	Aperture Scan Definition
3	0	null 5000
3	0	1
  - Aperture Table:**

Def#	Type	Param #1	Param #2	Param #3	Param #4	Param #5	Param #6	Param #7
1	rect	-100	-100	100	110	X	25	Y
  - Scan Program Table:**

Command	Arguments
VelNext	25
Y	-100
VelNext	50
X	-100
Z1	250
AZ	0
  - Control Panel:**
    - Current Laser Class:** Class I. Buttons: Start Test, Pause Test, Stop Test.
    - Test Operator:** [Text Field]. **Current Program Status:** Severe. **Abort Motion:** (Red button).
    - Test Comment:** [Text Field].
    - Test Status:** [Text Field].
    - Current Position:** Z: 250.00, Y: 0.00, X: -40.00, POL: -0.00, AZ: -0.00, [Empty].
    - Indicators:** Scan Active (Green dot), Stage Moving (Green dot), Stage Fault (Green dot).
- Footer:** SLDD v13.lvrproj/My Computer | File Format Error [Green dot] Error Line

The Test specification tab allows for loading a test specification from a file and displays the programs interpretation of the specification.

# Example test specification

```
// sample SLDD test specification file  
# 21 July 2012
```

```
Begin Test Header  
Test Name, Sample Test  
Test Creator, Armand Sperduti  
Test Comment  
UUT Name, Test Telescope  
UUT Model Number, 123456  
UUT Serial Number, SN4321
```

```
End Test Header
```

```
Begin FOV Table  
0 0 null 100  
.5 5 1  
.5 10 point 34.5 139.2 100  
.5 15 1  
.5 340 1  
.5 350 1  
1.0 340 1  
15.0 0 2  
15.0 10 2  
End FOV Table
```

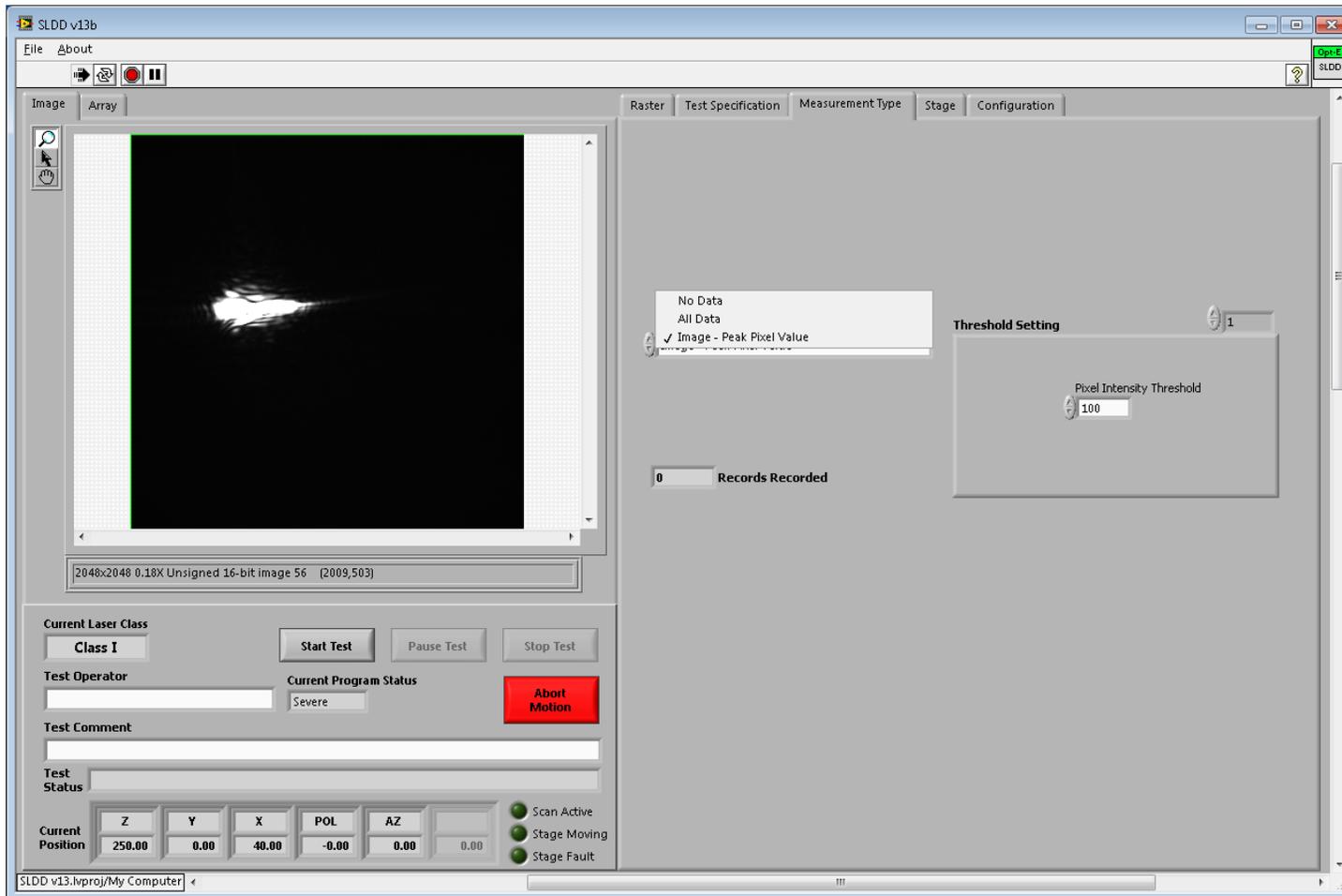
```
Begin Aperture 1  
rect 33.5 150.0 290.5 350.0 25.0 X 5.0 Y 2  
End Aperture
```

```
Begin Aperture 2  
vert 33.5 150.0 290.5 2  
End Aperture
```

```
Begin Scan Definition  
z1 50.5  
process FOV Table  
End Scan Definition
```

# SLDD program – Measurement type

Live Video



Status

The Measurement type is the operation performed on each image to determine if the image, or processed result, should be saved. The basic test is any pixel above a threshold value, although additional choices can be readily implemented in LabVIEW.

# SLDD program – Stage – manual control

Live Video

Status

The screenshot shows the SLDD v13b software interface. On the left, there is a 'Live Video' window displaying a dark image with a bright spot. Below it is a status panel with fields for 'Current Laser Class' (Class I), 'Test Operator', 'Test Comment', and 'Test Status'. It also shows 'Current Program Status' as 'Severe' and a red 'Abort Motion' button. At the bottom left, a 'Current Position' table displays values for Z (250.00), Y (0.00), X (-40.00), POL (-0.00), AZ (-0.00), and an unlabeled axis (0.00). The main control area on the right is titled 'Manual Control' and contains a table of 'Axis Values' and 'Axis Controls' for six axes: Z, Y, X, POL, AZ, and an unlabeled axis. The 'Axis Values' table shows Position and Velocity for each axis, along with status indicators for Enabled, Homed, Fault, and In Motion. The 'Axis Controls' table includes buttons for Disable, Home, Move To, Step, Jog, and Set Offset, along with numerical input fields for Move To Pos, Step Size, and Jog Velocity. A legend at the bottom right explains the 'Set Offset' function.

Name	Name	Name	Name	Name	Name
Z	Y	X	POL	AZ	
Position	Position	Position	Position	Position	Position
250.0000	0.0000	40.0000	-0.0007	-0.0009	0.0000
Velocity	Velocity	Velocity	Velocity	Velocity	Velocity
0.0000	0.0000	0.0001	-0.0069	-0.0368	0.0000
Enabled	Enabled	Enabled	Enabled	Enabled	Enabled
Homed	Homed	Homed	Homed	Homed	Homed
Fault	Fault	Fault	Fault	Fault	Fault
In Motion					

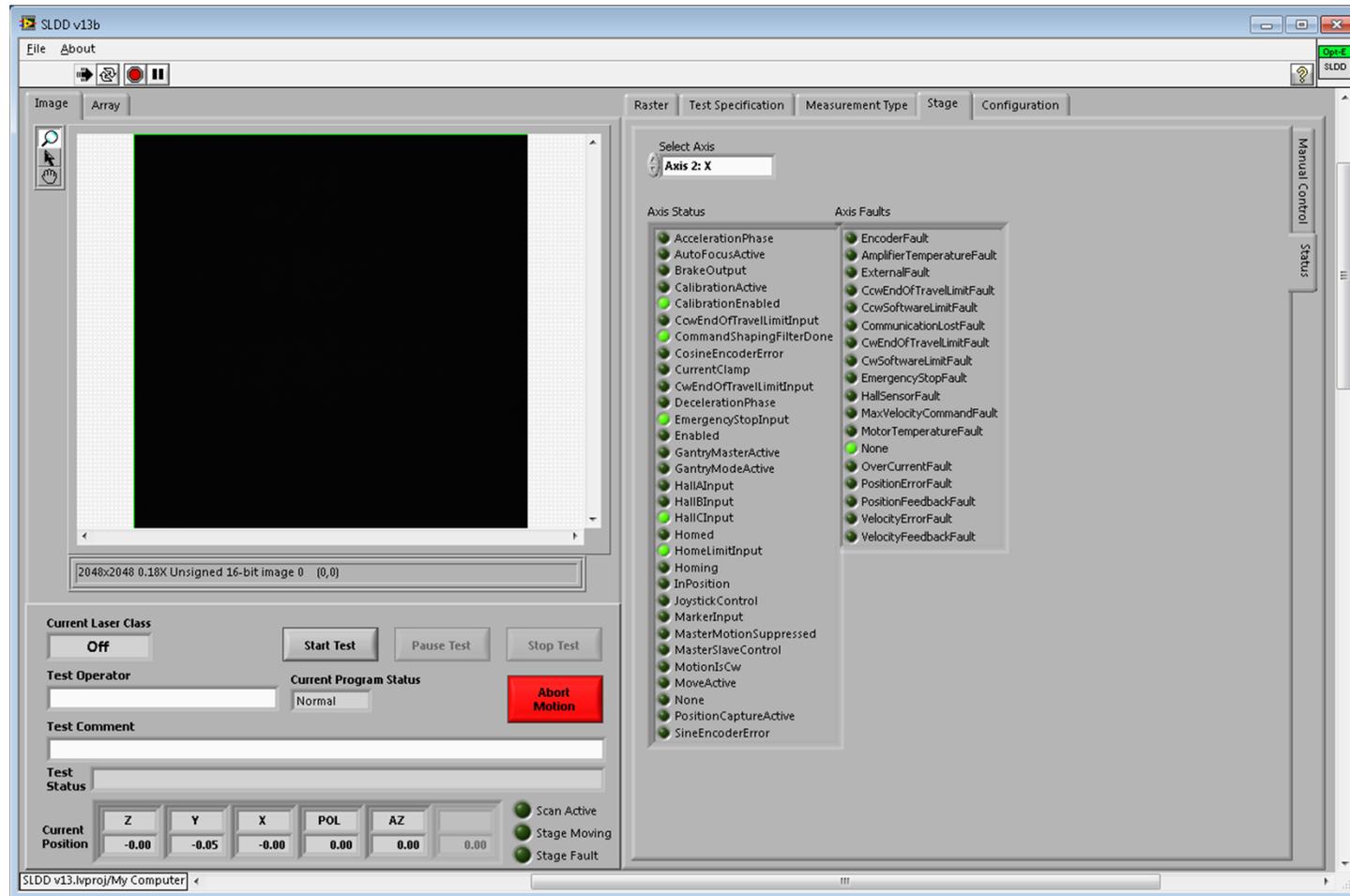
Disable	Disable	Disable	Disable	Disable	Enable
Home	Home	Home	Home	Home	Home
Move To					
Move To Pos					
250.00	0.00	0.00	0.00	0.00	0.00
Step -					
Step +					
Step Size					
0.000	1.000	1.000	0.050	1.000	0.000
Jog -					
Jog +					
Jog Velocity					
10.000	25.000	25.000	0.500	15.000	0.000
Ack Fault					
Home Offset					
0.000	-119.211	134.611	0.740	-134.484	0.000
Set Offset	Set Home				

Stage → manual control provides necessary controls for setup operations. Full status information from the Aerotech Ensemble controller is available on a second tab.

# SLDD program – Stage – status

Live Video

Status

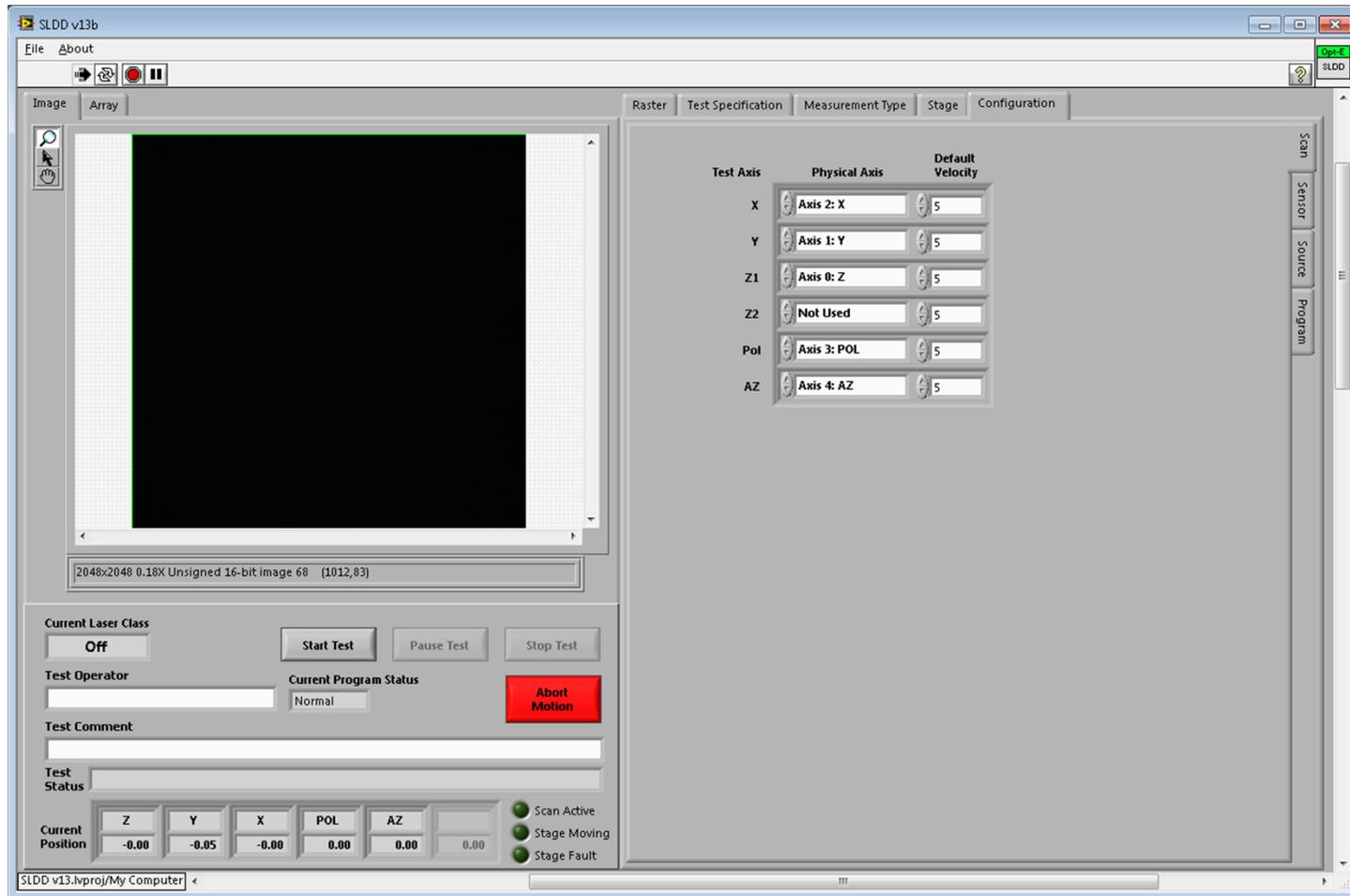


Stage → status provides complete status information by axis.

# SLDD program – Configuration - Scan

Live Video

Status

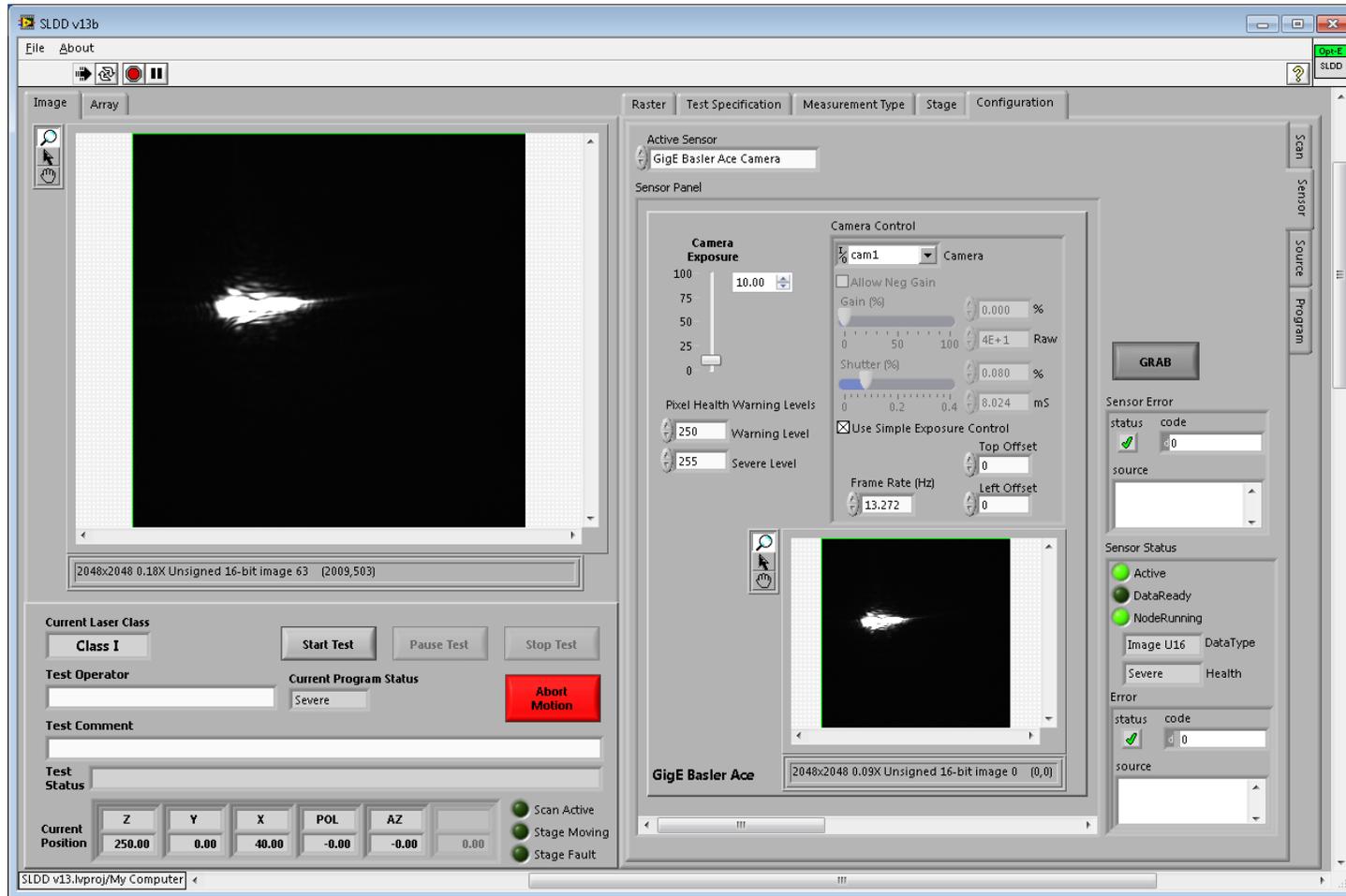


Configuration → Scan sets the velocities for the Raster test.

# SLDD program – Configuration - Sensor

Live Video

Status

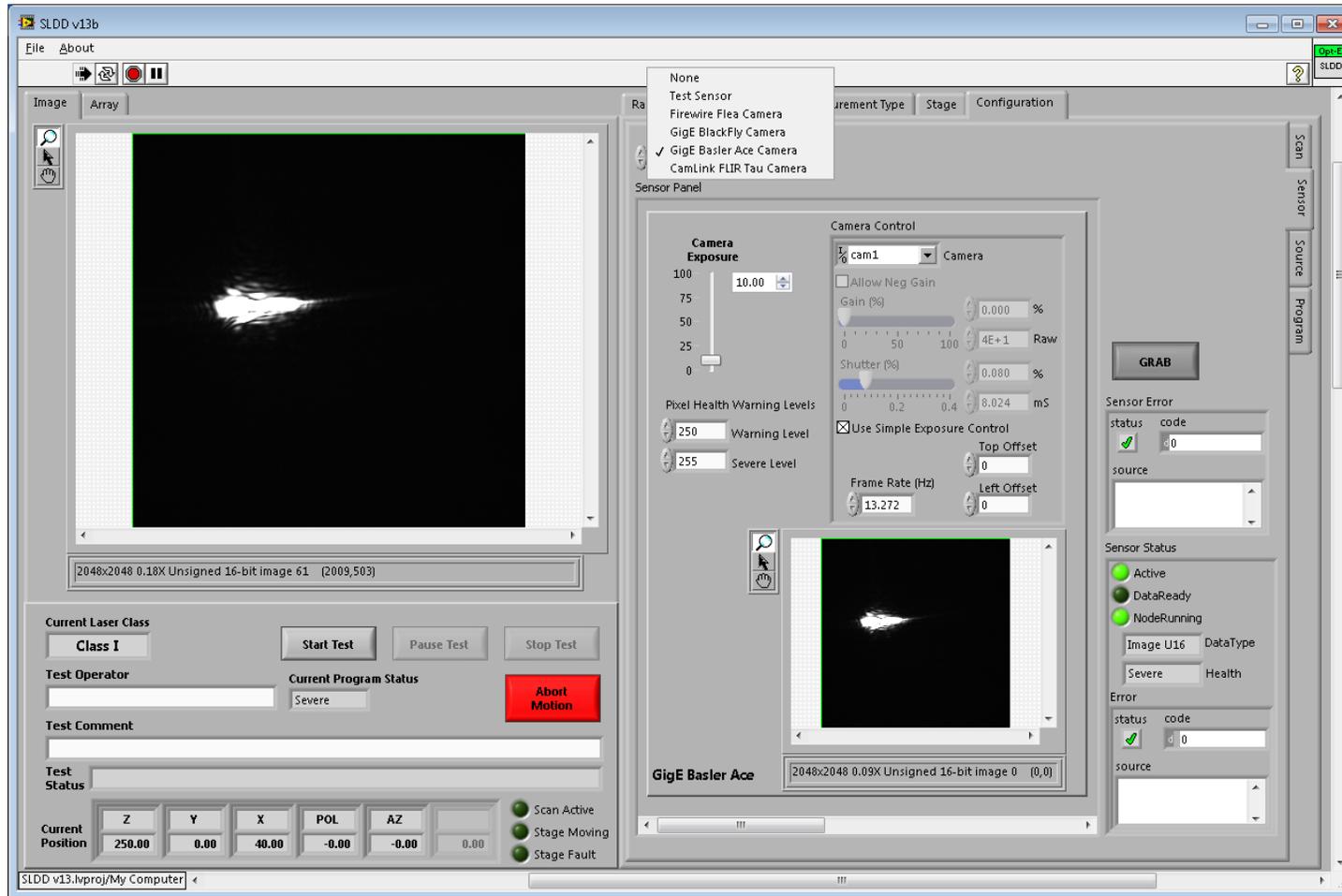


Configuration → Sensor provides access to the sensor sub-panel for the sensor “Active Node”. The sensor interface is a stand alone program loaded in a subpanel that provides detailed control. The Active Node approach allows for interfaces to virtually any standard or custom sensor to be implemented.

# SLDD program – Configuration - Sensor

Live Video

Status

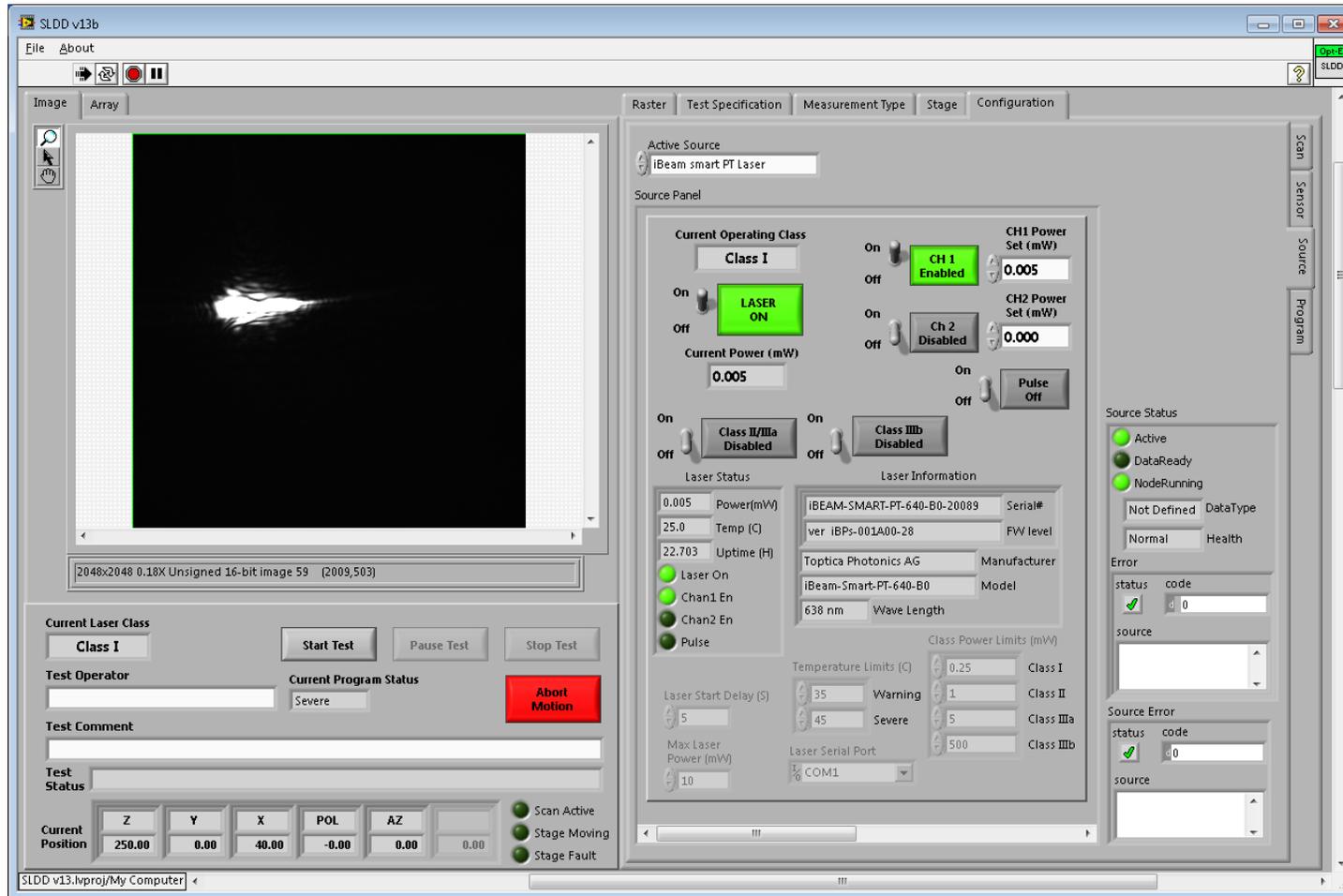


Configuration → Sensor provides access to the sensor sub-panel for the sensor “Active Node”. The sensor interface is a stand alone program loaded in a subpanel that provides detailed control. The Active Node approach allows for interfaces to virtually any standard or custom sensor to be implemented.

# SLDD program – Configuration - Source

Live Video

Status



Configuration → Source provides access to the sensor sub-panel for the source “Active Node”. The source interface is a stand alone program loaded in a subpanel that provides detailed control. The Active Node approach allows for interfaces to virtually any standard or custom source to be implemented.

# SLDD program – Configuration - Source

Live Video

Status

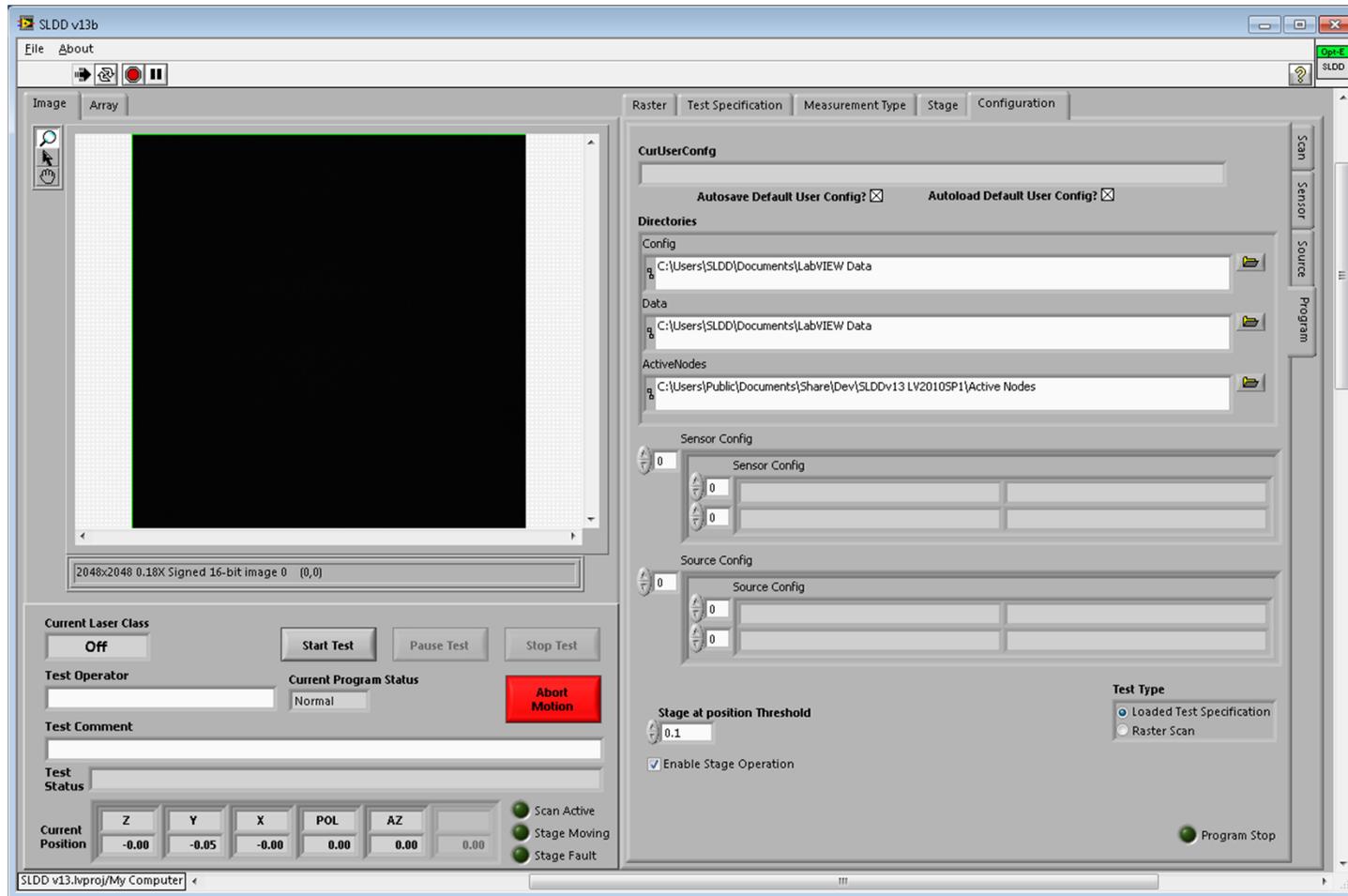


Configuration → Source provides access to the sensor sub-panel for the source “Active Node”. The source interface is a stand alone program loaded in a subpanel that provides detailed control. The Active Node approach allows for interfaces to virtually any standard or custom source to be implemented.

# SLDD program – Configuration - Program

Live Video

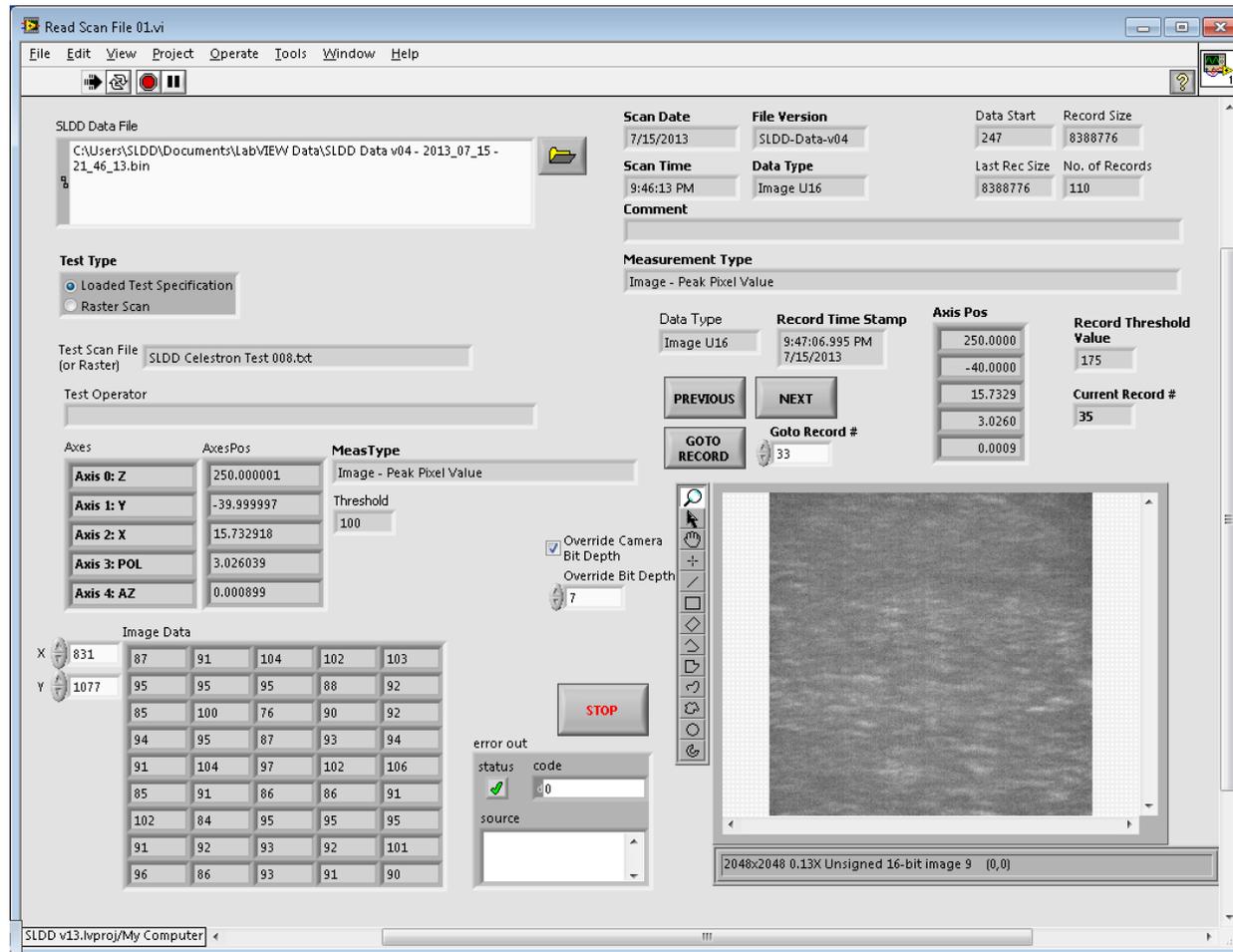
Status



Configuration → Program provides access to file directory specifications and other necessary stuff.



# Read Scan File (2)



SLDD saves image data and Read Scan File allows for examination of the data. It is intended to be modified for further analysis. It is easy to write equivalent programs in any environment, such as Matlab. Data is from the Celestron C-8 amateur telescope with a Basler Ace camera attached.

# Read Scan File (3)



SLDD saves image data and Read Scan File allows for examination of the data. It is intended to be modified for further analysis. It is easy to write equivalent programs in any environment, such as Matlab.

Data is from the Celestron C-8 amateur telescope with a Basler Ace camera attached.

## What else to do?

- A control program to control filling of the cryogenic tanks needs to be written for the cryogenic beam dump.
- We are preparing to test the cryogenic beam dump in September.
- We will test two IR&D telescopes at atmospheric temperature at both wavelengths this fall.
- There are some miscellaneous hardware things to add such as AC power feeds, adding a shelf for the Aries laser controller, etc.
- There are incremental software improvements and additions needed, as is usually true.
- Presentations or publications on measurement results compared with analyses, at least as possible, are also needed.
- We are looking to use this instrument, so please, talk to me. We can couple with stray light analysis if useful.

**Backup slides follow**

# 295 K BB, 0.03 e, 8-12 $\mu\text{m}$ (mirror)

SpectralCalc - 295K 0.03 e 8-12 um.pdf - Adobe Acrobat Pro

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### Blackbody Calculator

Inputs		Results	
<b>Units:</b> Watts Wavelength ( $\mu\text{m}$ ) Kelvin			
<b>Blackbody Properties:</b> Temperature: 295 K Emissivity: .03 Recession Velocity: 0 km/s		Radiant emittance: 12.8835 $\text{W/m}^2$ Radiance: 4.10093 $\text{W/m}^2/\text{sr}$ Peak spectral radiance: 0.274518 $\text{W/m}^2/\text{sr}/\mu\text{m}$ Wavelength of peak: 9.82289 $\mu\text{m}$	
Wavelength: 10 $\mu\text{m}$		Spectral Radiance: 0.274308 $\text{W/m}^2/\text{sr}/\mu\text{m}$ (5.03412e+19 photons/J)	
Lower Limit: 8 $\mu\text{m}$ Upper Limit: 12 $\mu\text{m}$		Band Radiance: 1.06295 $\text{W/m}^2/\text{sr}$	

# 295 K BB, 1 e, 8-12 $\mu\text{m}$ (beam dump)

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**Blackbody Calculator**

Inputs		Results	
<b>Units:</b>			
Watts	<input type="text"/>		
Wavelength ( $\mu\text{m}$ )	<input type="text"/>	Radiant emittance:	429.449 $\text{W/m}^2$
Kelvin	<input type="text"/>	Radiance:	138.898 $\text{W/m}^2/\text{sr}$
<b>Blackbody Properties:</b>		Peak spectral radiance:	0.15081 $\text{W/m}^2/\text{sr}/\mu\text{m}$
Temperature:	295 K	Wavelength of peak:	9.82289 $\mu\text{m}$
Emissivity:	1		
Recession Velocity:	0 km/s		
Wavelength <input type="text"/> $\mu\text{m}$		Spectral Radiance:	0 $\text{W/m}^2/\text{sr}/\mu\text{m}$ (0 photons/J)
Lower Limit	8 $\mu\text{m}$		
Upper Limit	12 $\mu\text{m}$	Band Radiance:	35.4317 $\text{W/m}^2/\text{sr}$

# 100 K BB, 1.0 e, 8-12 $\mu\text{m}$ (beam dump)

SpectralCalc - 100K 1.0 e 8-12 um.pdf - Adobe Acrobat Pro

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**Blackbody Calculator**

Inputs		Results	
<b>Units:</b> Watts Wavelength ( $\mu\text{m}$ ) Kelvin			
<b>Blackbody Properties:</b> Temperature: 100 K Emissivity: 1 Recession Velocity: 0 km/s		Radiant emittance: 5.67052 $\text{W/m}^2$ Radiance: 1.80498 $\text{W/m}^2/\text{sr}$ Peak spectral radiance: 0.0409581 $\text{W/m}^2/\text{sr}/\mu\text{m}$ Wavelength of peak: 28.9775 $\mu\text{m}$	
Wavelength 0 $\mu\text{m}$		Spectral Radiance: 0 $\text{W/m}^2/\text{sr}/\mu\text{m}$ (0 photons/J)	
Lower Limit 8 $\mu\text{m}$ Upper Limit 12 $\mu\text{m}$		Band Radiance: 0.00382278 $\text{W/m}^2/\text{sr}$	

# 77.35 K BB, 1.0 e, 8-12 $\mu\text{m}$ (beam dump)

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**Blackbody Calculator**

Inputs		Results	
<b>Units:</b> Watts <input type="text"/> Wavelength ( $\mu\text{m}$ ) <input type="text"/> Kelvin <input type="text"/>		Radiant emittance: 2.02985 $\text{Wm}^2$ Radiance: 0.846122 $\text{Wm}^2/\text{sr}$ Peak spectral radiance: 0.0113407 $\text{Wm}^2/\text{sr}/\mu\text{m}$ Wavelength of peak: 37.4829 $\mu\text{m}$	
<b>Blackbody Properties:</b> Temperature: 77.35 K Emissivity: 1 Recession Velocity: 0 km/s			
Wavelength 0 <input type="text"/> $\mu\text{m}$		Spectral Radiance: 0 $\text{Wm}^2/\text{sr}/\mu\text{m}$ (0 photons/J)	
Lower Limit 8 <input type="text"/> $\mu\text{m}$ Upper Limit 12 <input type="text"/> $\mu\text{m}$		Band Radiance: 8.3721e-05 $\text{Wm}^2/\text{sr}$	

# 6000 K BB, 1.0 e, 8-12 $\mu\text{m}$ (sun)

SpectralCalc - 6000K 1.0 e 8-12 um.pdf - Adobe Acrobat Pro

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**Blackbody Calculator**

Inputs		Results	
<b>Units:</b> Watts Wavelength ( $\mu\text{m}$ ) Kelvin			
<b>Blackbody Properties:</b> Temperature: 6000 K Emissivity: 1 Recession Velocity: 0 km/s		Radiant emittance: $7.349\text{e}+07 \text{ W/m}^2$ Radiance: $2.33926\text{e}+07 \text{ W/m}^2/\text{sr}$ Peak spectral radiance: $3.1849\text{e}+07 \text{ W/m}^2/\text{sr}/\mu\text{m}$ Wavelength of peak: $0.482959 \mu\text{m}$	
Wavelength: 10 $\mu\text{m}$		Spectral Radiance: $4395.19 \text{ W/m}^2/\text{sr}/\mu\text{m}$ (5.03412e+19 photons/J)	
Lower Limit: 8 $\mu\text{m}$ Upper Limit: 12 $\mu\text{m}$		Band Radiance: $19964.7 \text{ W/m}^2/\text{sr}$	

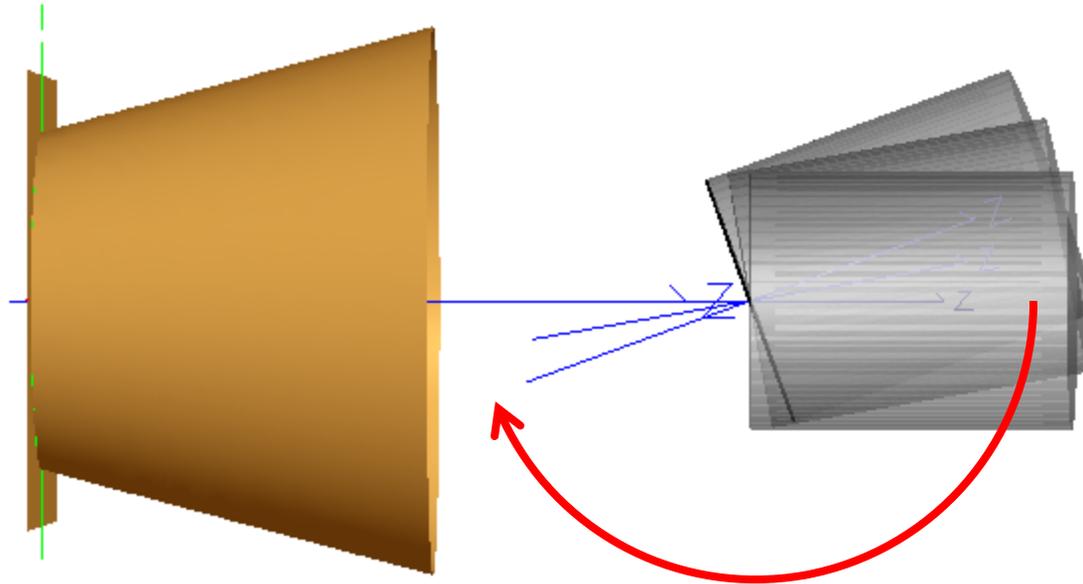


# Baffle PST Trades

Richard N. Pfisterer  
Photon Engineering

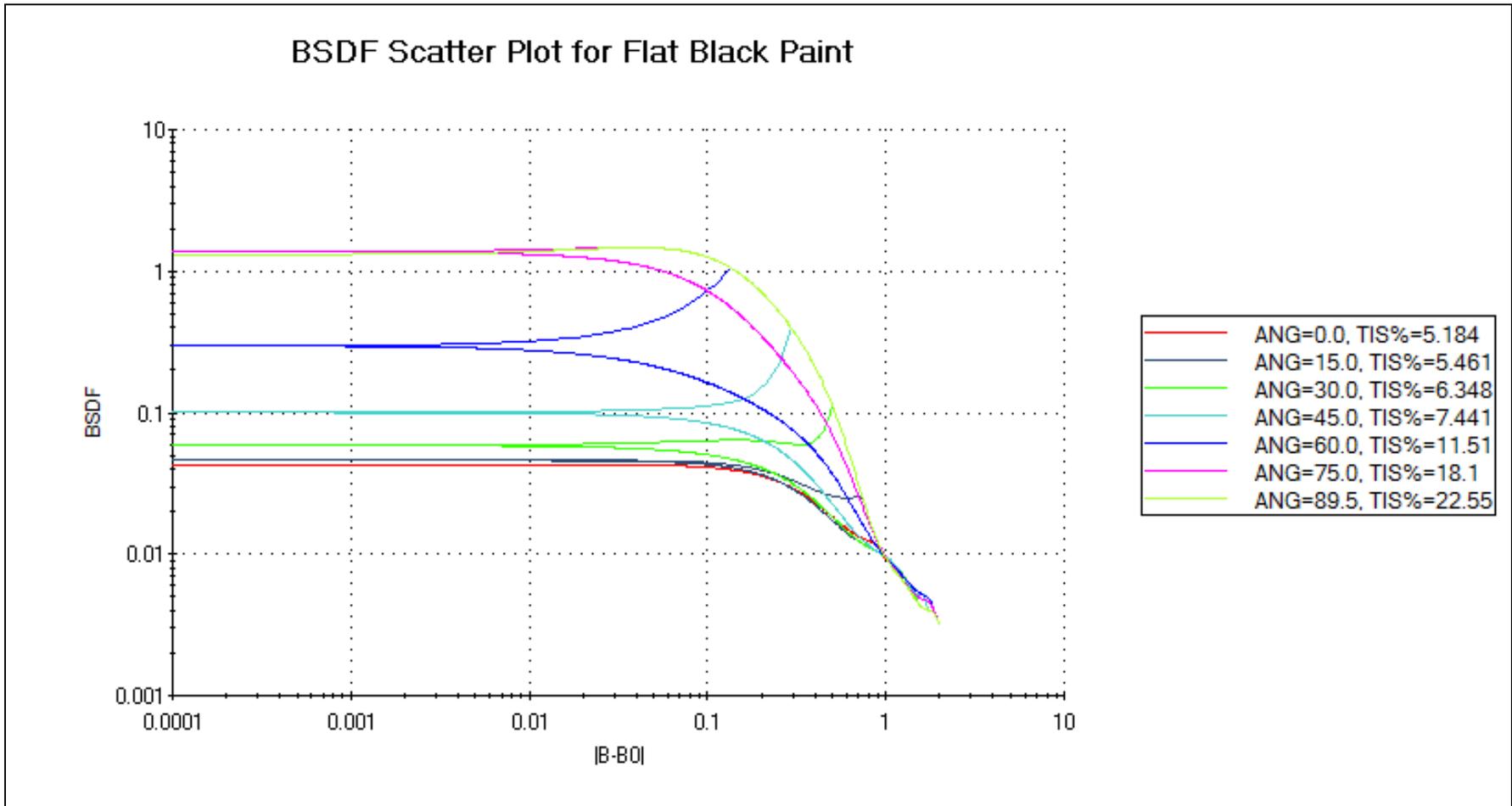
Revised 16 Nov 2011

## Analysis Technique

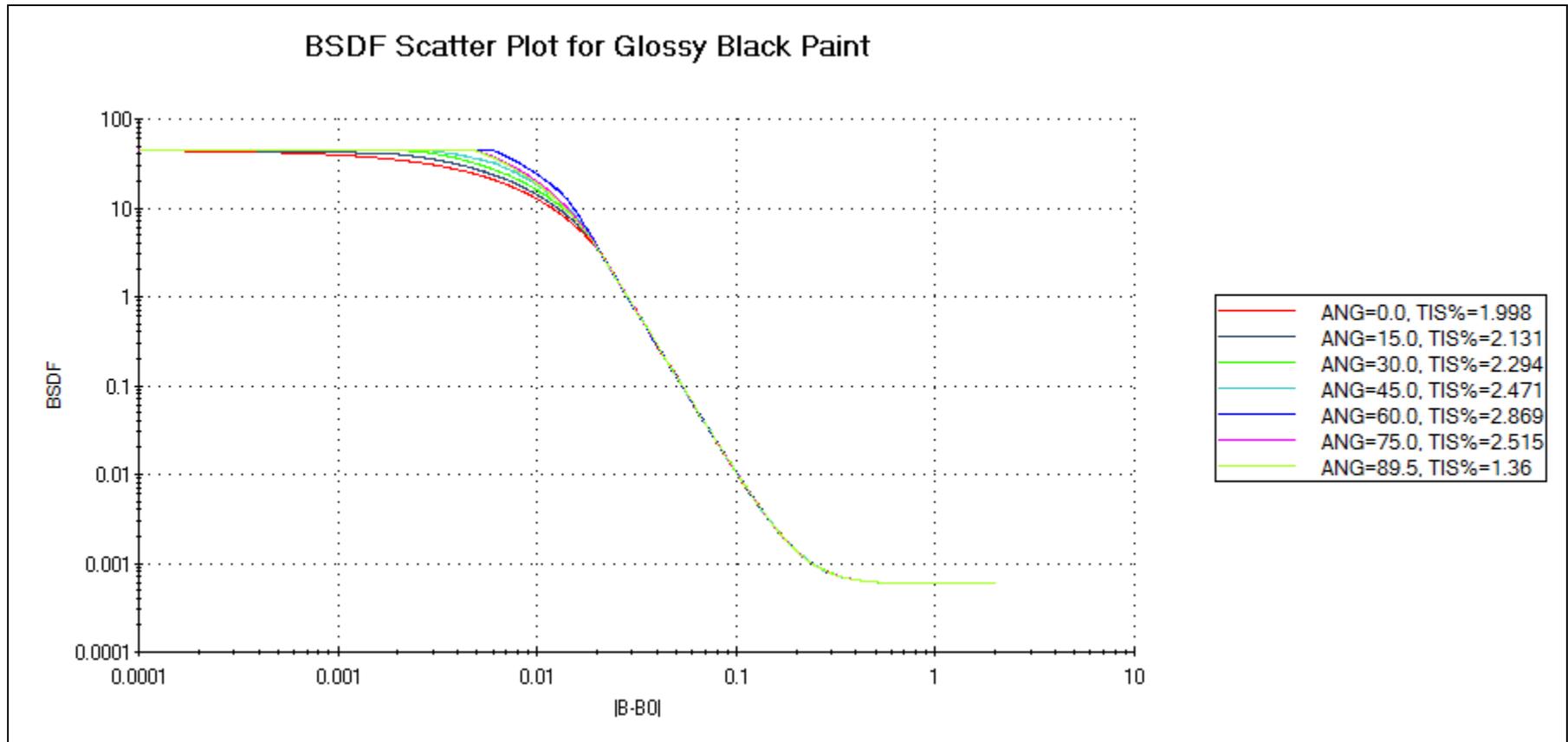


1. System under test is rotated about a fixed point in front of the baffle
2. Rays are traced from the system under test into a  $\pm 2$  deg FOV. The source power is set to unity.
3. Rays are scattered back to the entrance aperture of the system under test
4.  $PST = (\text{scatter power collected on entrance aperture}) / (\text{power emitted by entrance aperture})$

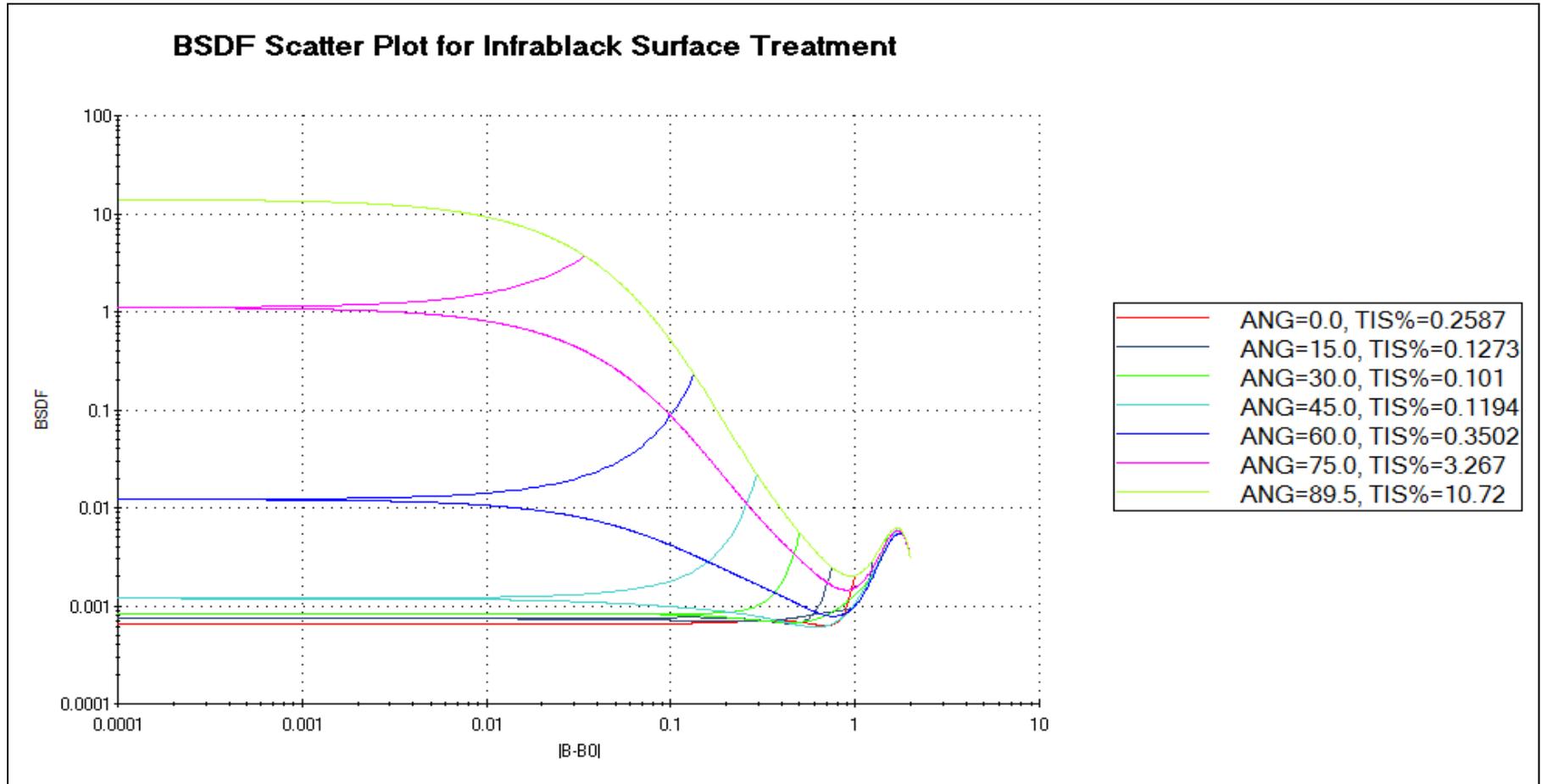
Visible Flat Black Scatter Model



## Visible Glossy Black Scatter Model

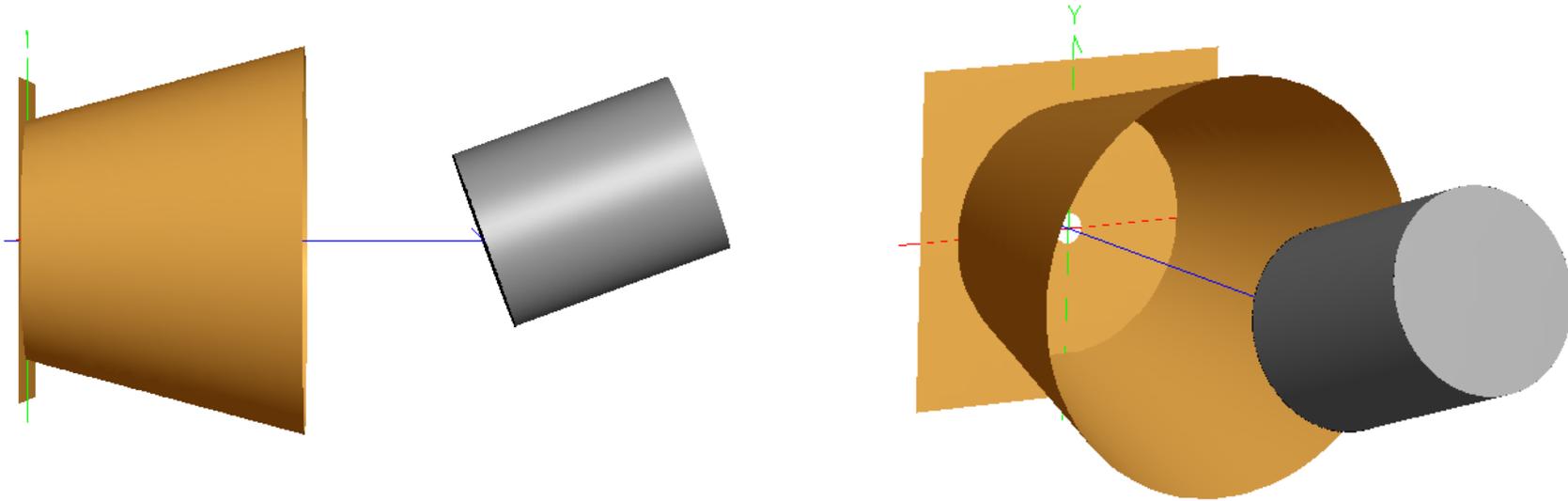


## LWIR Flat Black Scatter Model



Infrablack is a surface treatment for aluminum that is optimized for the LWIR. Note that it is an order of magnitude less scattering than Z306, the “generic” flat black paint used in the visible; this is typical of black surface treatments in the LWIR. (See comments)

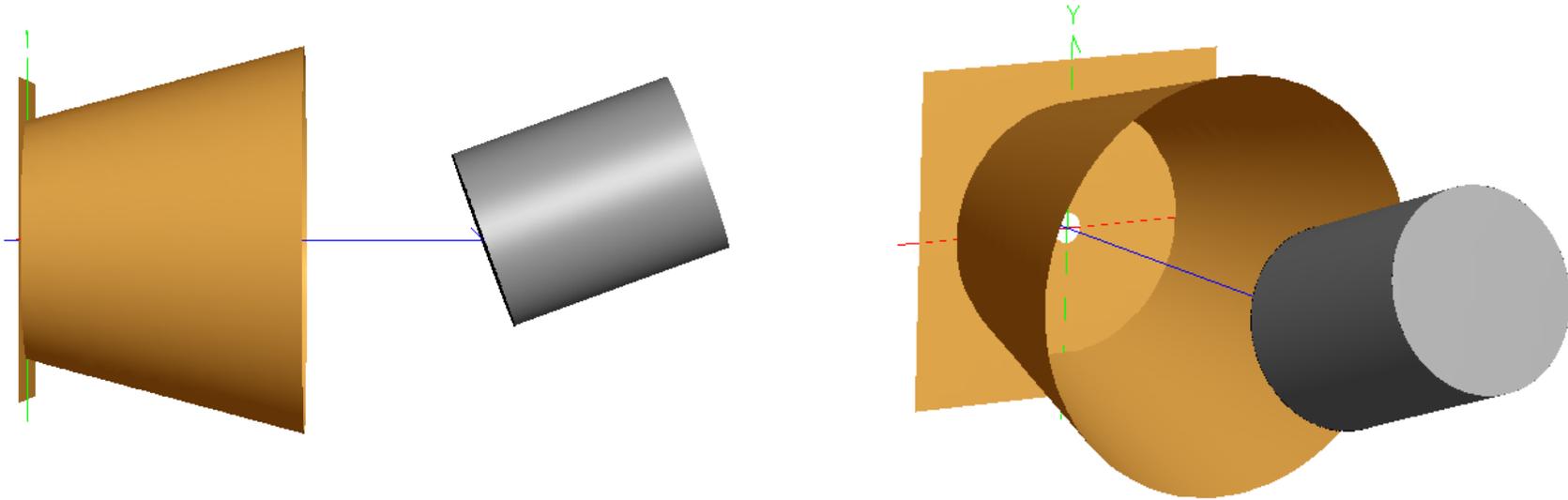
## Simple Cone w/Flat Black Paint (Visible)



angle	PST
0	4.17E-03
5	3.58E-03
10	2.23E-03
15	1.27E-03
20	8.27E-04

Nothing exciting is happening here; this is the baseline calculation. Basically we're looking at the scatter from a flat (diffuse) black surface.

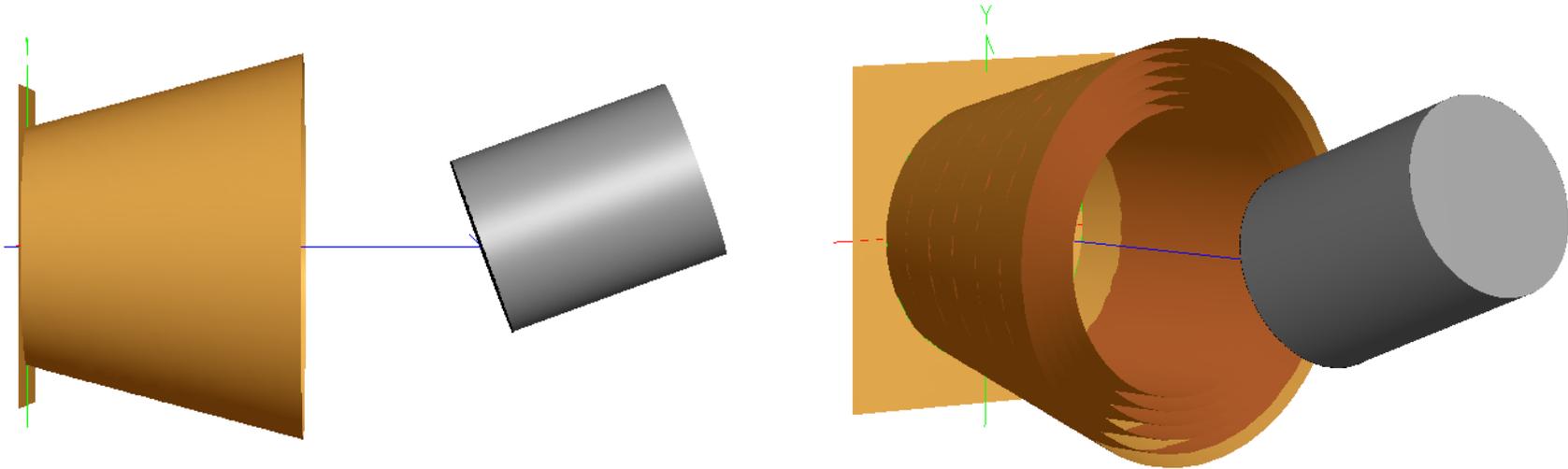
## Simple Cone w/Gloss Black Paint (Visible)



angle	PST
0	1.45E-02
5	7.81E-03
10	7.45E-04
15	6.70E-05
20	6.73E-05

Note that the near-normal PST is an order of magnitude higher than the flat black. This is due to the high specularity of the gloss paint creating a near-retro reflection back to the system under test. However once the system is tilted such that the reflection is outside the FOV, the PST drops an order of magnitude.

## Simple Cone w/Cylindrical Baffles and Flat Black Paint (Visible)

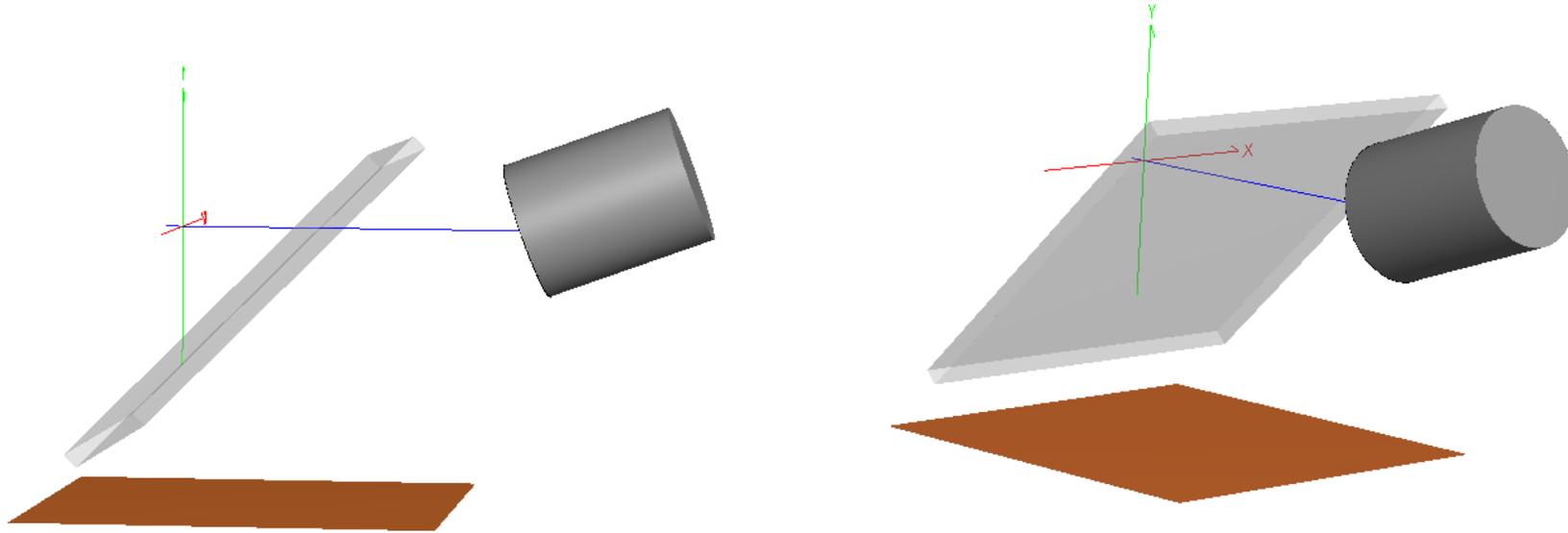


angle	PST
0	4.15E-03
5	3.56E-03
10	2.21E-03
15	1.26E-03
20	6.98E-04

There is not much difference in the PST between the flat black cone and the cone w/cylindrical baffles because the geometry really isn't much different: at normal incidence the system under test is looking at the same flat surface and at higher angles of incidence, it is looking at another conical surface.

Based on these results, I don't expect to see anything significantly different if we angled the cylindrical baffles.

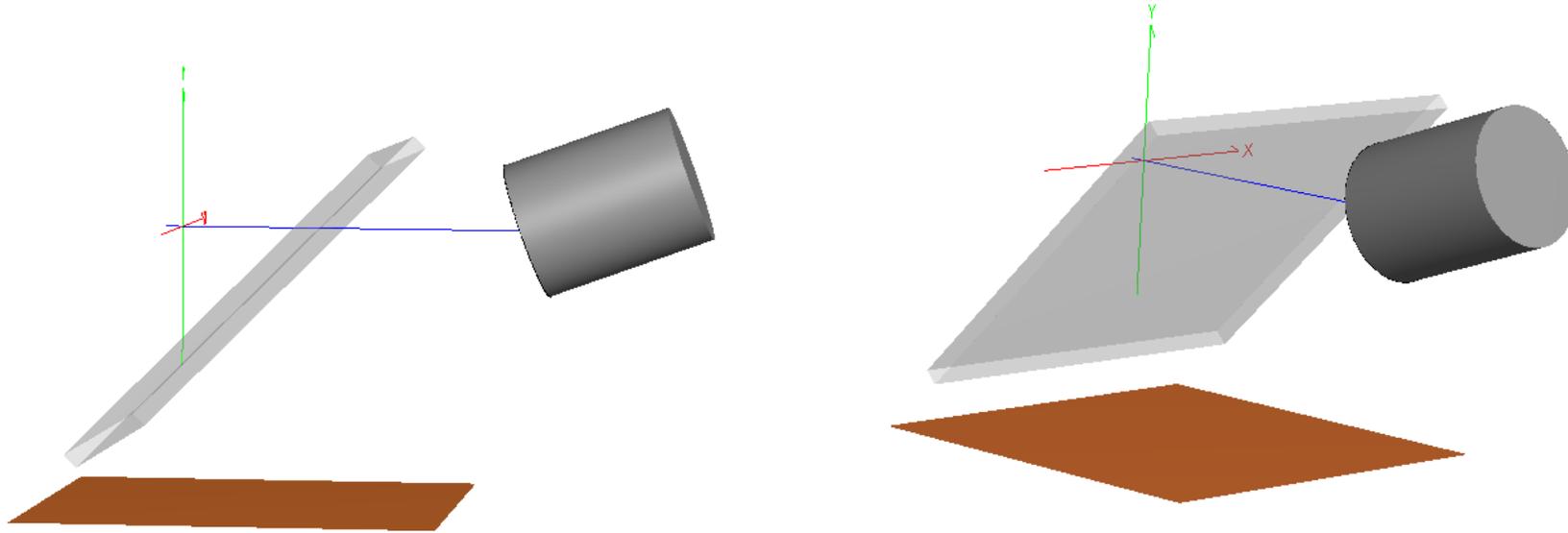
## Stage 1 Baffle w/Black Glass and Flat Black Paint Absorber (Visible)



angle	PST
0	8.61E-05
5	7.63E-05
10	6.91E-05
15	6.05E-05
20	5.36E-05

Note the significant improvement over the flat black paint baffles! I assumed a visibly dirty glass plate (level 500) and a 17 angstrom rms roughness surface.

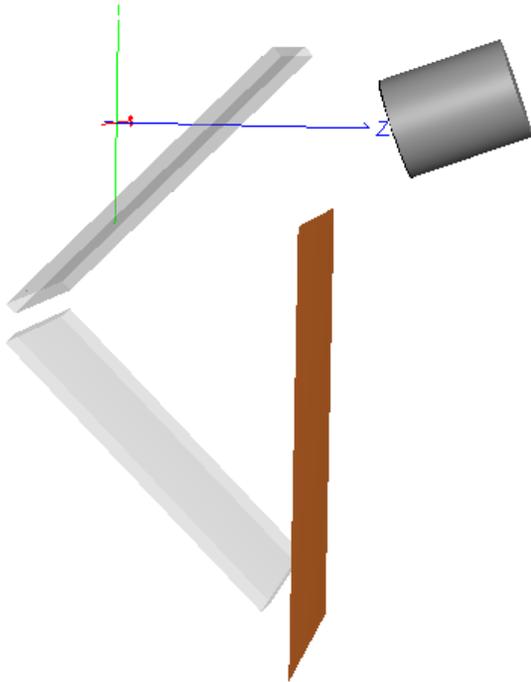
## Stage 1 Baffle w/Black Glass and Flat Black Paint Absorber (no particles on glass, Visible)



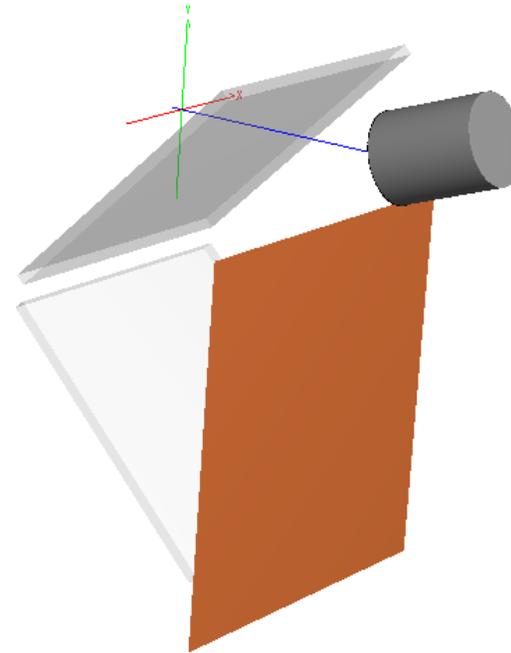
angle	PST (no particles)
0	3.76E-05
5	2.84E-05
10	2.05E-05
15	1.46E-05
20	1.02E-05

It is tempting to consider how good the stage 1 baffle could be if you could eliminate the particles. At small angles, the PST is a factor of 2x lower; at larger angles it is better by a factor of 5x.

## Stage 2 Baffle w/Black Glass and Flat Black Paint Absorber (Visible)

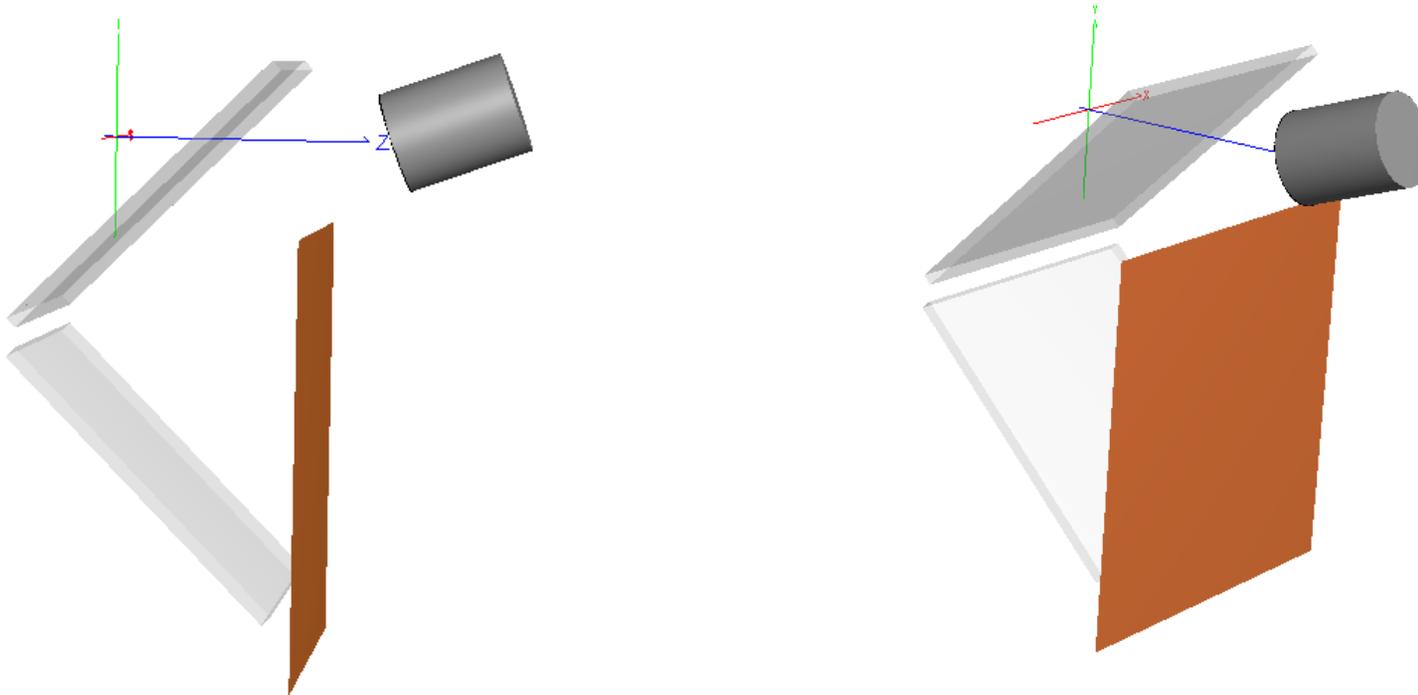


angle	PST
0	5.52E-05
5	4.77E-05
10	4.34E-05
15	4.11E-05
20	3.80E-05



You'll notice that the stage 2 baffle is virtually identical to the stage 1 baffle, despite the increase in complexity. This is due to the significant contribution from particulate scatter on the first glass plate.

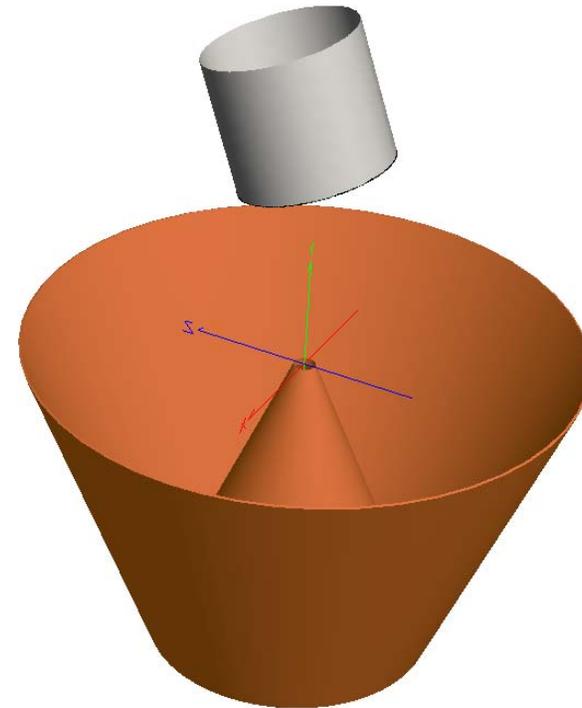
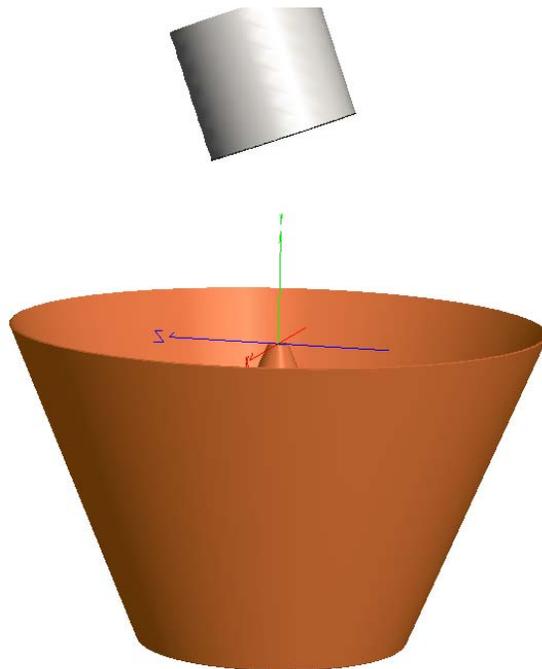
## Stage 2 Baffle w/Black Glass and Flat Black Paint Absorber (no particles on glass, Visible)



angle	PST (no particles)
0	1.26E-05
5	8.86E-06
10	5.81E-06
15	3.60E-06
20	2.13E-06

Without particles, we pick up a factor of 5x improvement at small angles, but an order of magnitude improvement at larger angles.

## Nested Cones w/Gloss Black Paint (Visible)

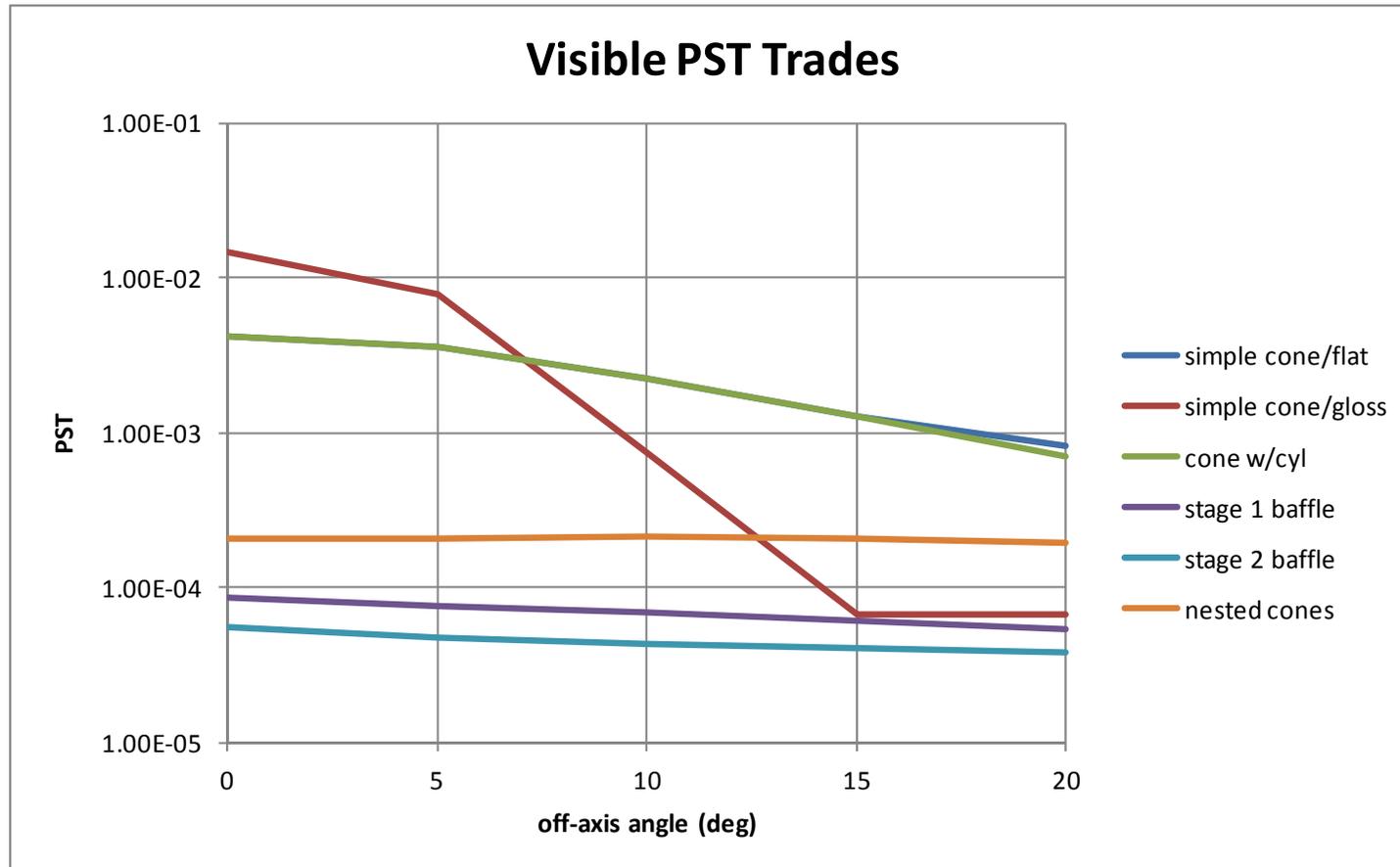


angle	PST
0	2.04E-04
5	2.05E-04
10	2.15E-04
15	2.07E-04
20	1.94E-04

A rather interesting “middle ground” between the conventional baffles and the stage 1 and 2 baffles.

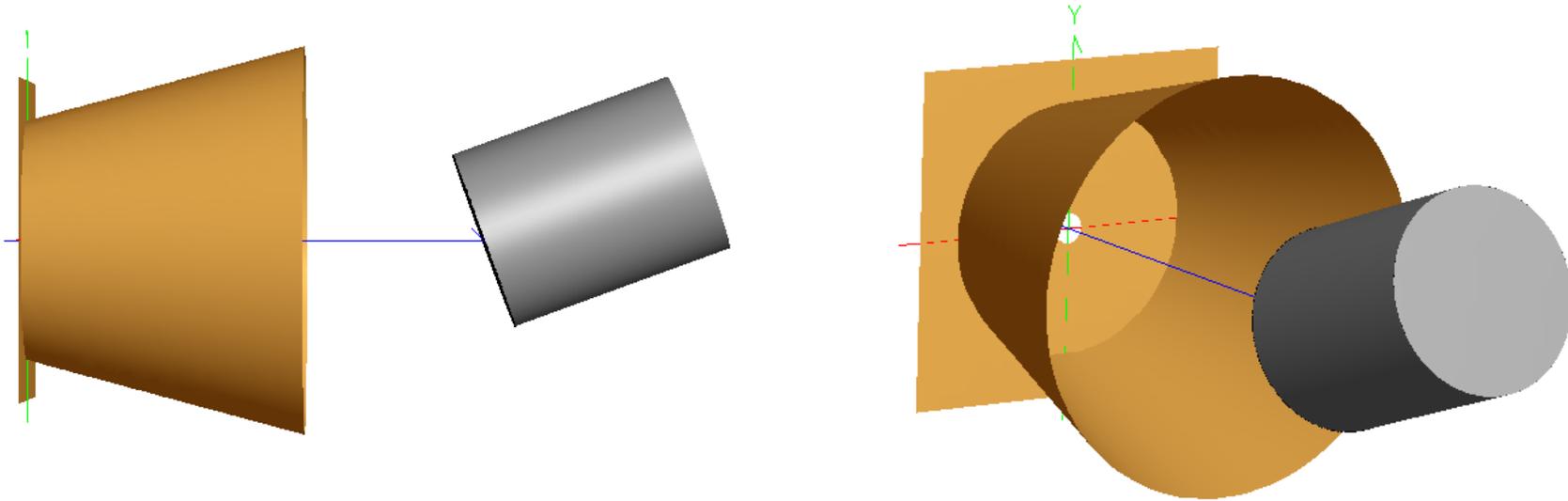
Fundamentally it is a conical cavity but the paint is glossy, so at each ray intersection with the surface, you have a specular reflection and a diffuse component.

## How do They Compare?



Note that the simple cone/flat and cone w/cyl are virtually identical except at larger angles.

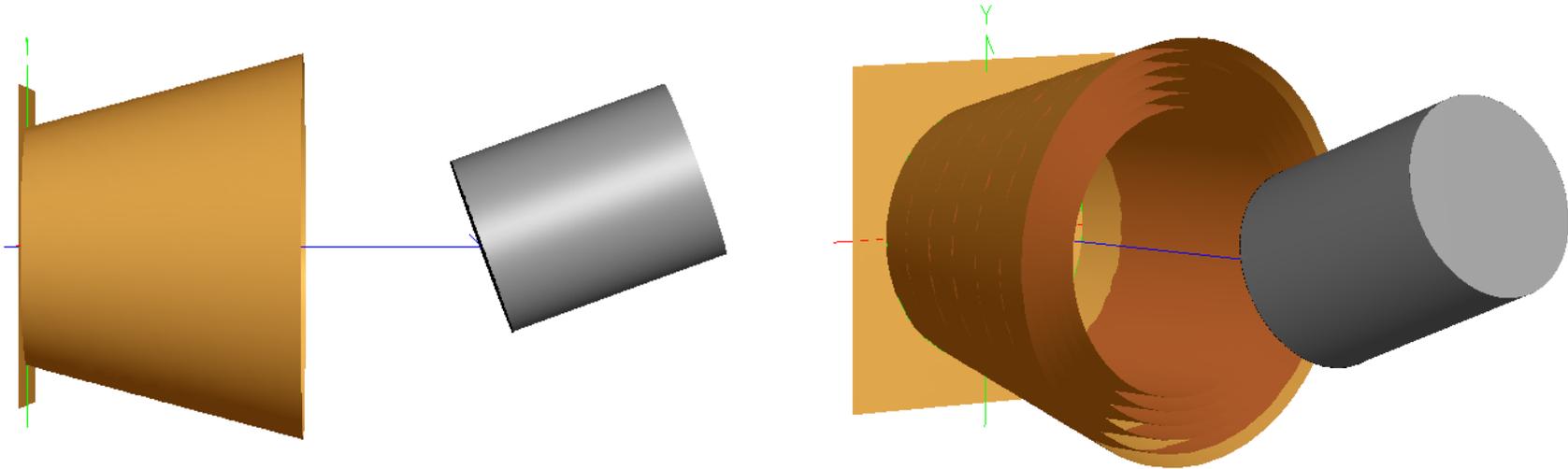
## Simple Cone w/Infrablack (LWIR)



angle	PST
0	1.08E-03
5	7.09E-04
10	3.03E-04
15	2.08E-04
20	2.16E-04

This is approx. 4x lower than for the visible but the scatter mechanism is completely different: in the visible, the paint scatter is the dominant mechanism; in the LWIR, particulates contaminating the paint dominate and the paint is an insignificant contributor.

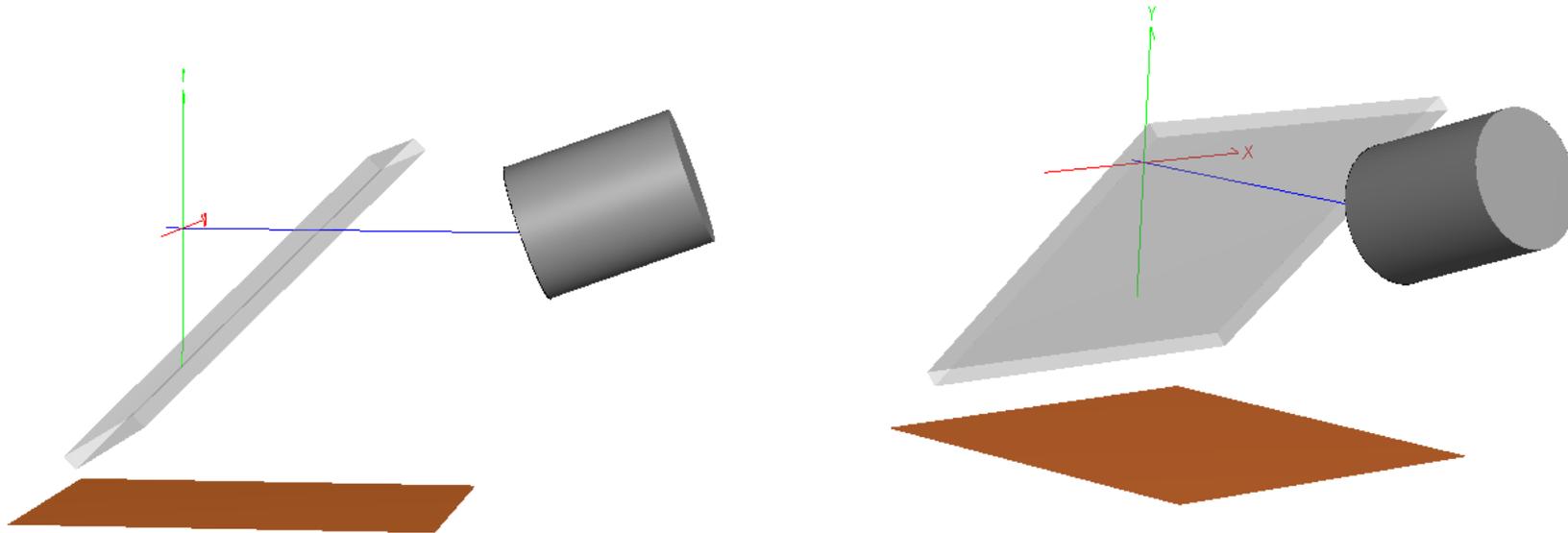
## Simple Cone w/Cylindrical Baffles and w/Infrablack (LWIR)



angle	PST
0	1.09E-03
5	6.85E-04
10	2.87E-04
15	1.74E-04
20	1.65E-04

As before, there is not much difference in the PST between the flat black cone and the cone w/cylindrical baffles because the geometry really isn't much different: at normal incidence the system under test is looking at the same flat surface and at higher angles of incidence, it is looking at another conical surface, both contaminated with particulates.

## Stage 1 Baffle w/Infrablack and w/Infrablack Absorber (LWIR)

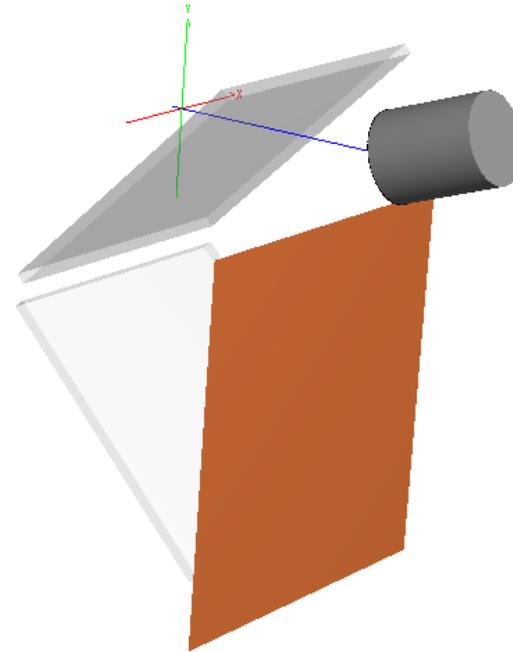
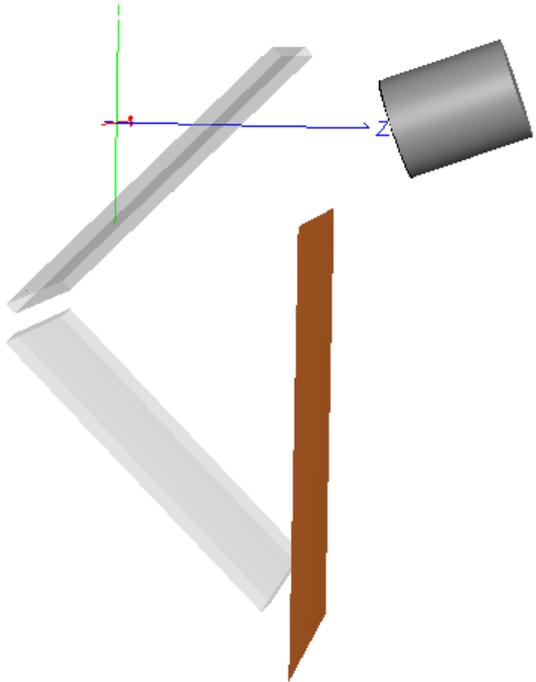


angle	PST
0	1.07E-05
5	9.34E-06
10	8.64E-06
15	8.14E-06
20	6.93E-06

Approx. 8x lower scatter than in the visible.

Note the significant improvement over the flat black paint baffles! I assumed a visibly dirty (Al?) panel (level 500) and a 17 angstrom rms roughness surface. However at this wavelength the surface scatter is entirely negligible.

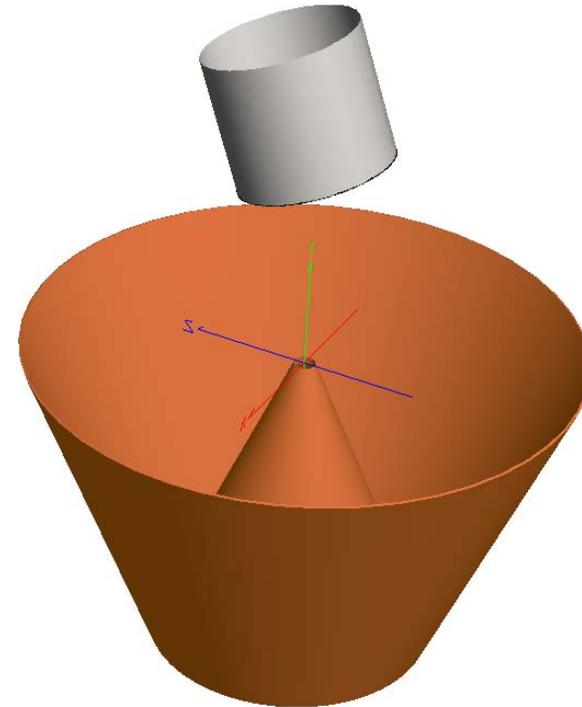
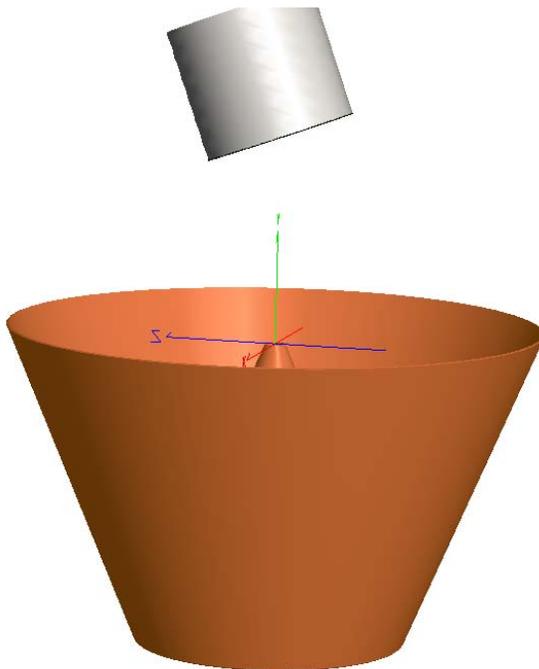
## Stage 2 Baffle w/Black Glass and w/Infrablack Absorber (LWIR)



angle	PST
0	9.77E-06
5	8.83E-06
10	7.71E-06
15	7.08E-06
20	6.13E-06

As before, you'll notice that the stage 2 baffle is virtually identical to the stage 1 baffle, despite the increase in complexity. This is due to the significant contribution from particulate scatter on the first panel.

## Nested Cones w/InfraBlack (LWIR)

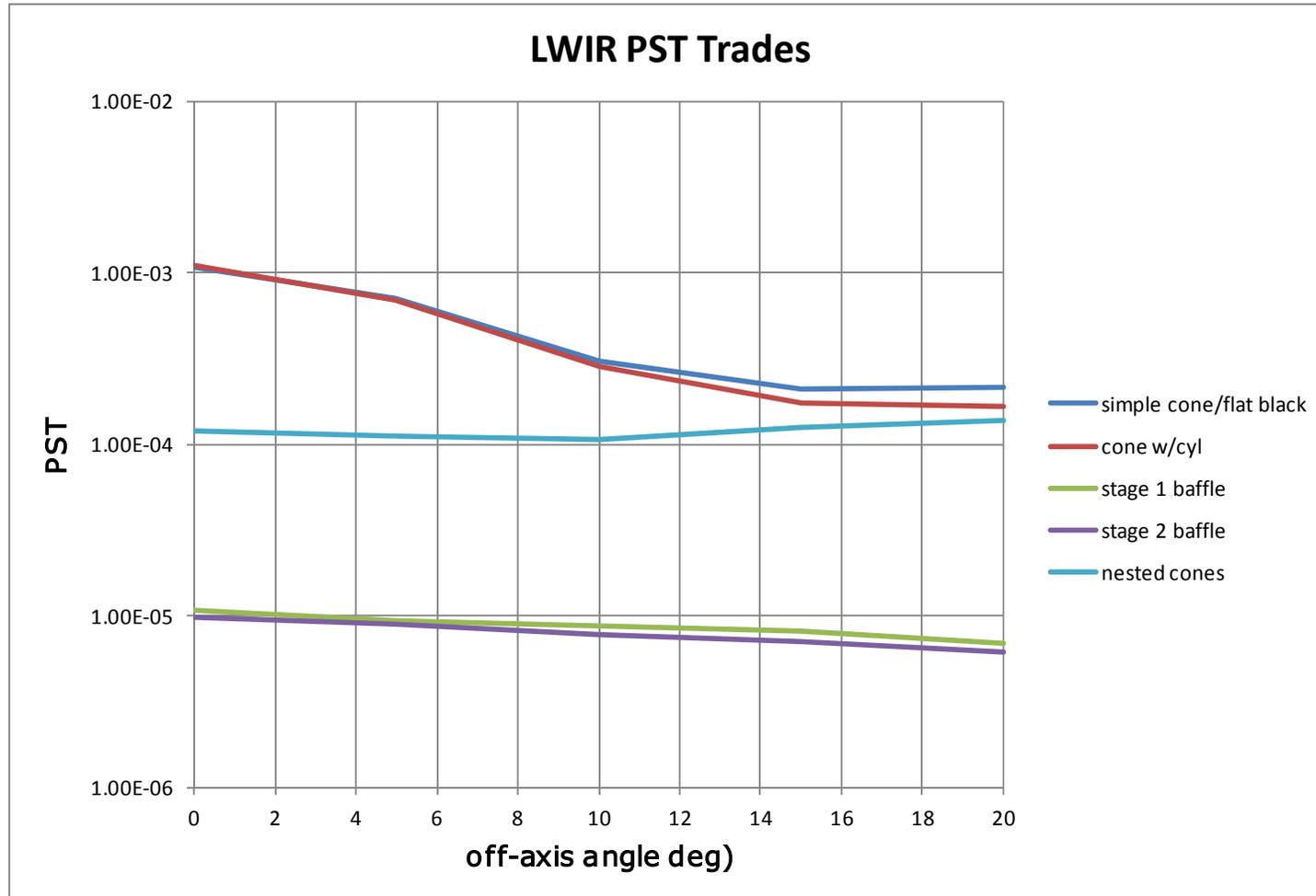


angle	PST
0	1.20E-04
5	1.11E-04
10	1.07E-04
15	1.25E-04
20	1.39E-04

A rather interesting “middle ground” between the conventional baffles and the stage 1 and 2 baffles.

Fundamentally it is a conical cavity but the paint is glossy, so at each ray intersection with the surface, you have a specular reflection and a diffuse component.

## How do They Compare?



Note that the simple cone/flat and cone w/cyl are virtually identical except at larger angles.

## Visible and LWIR PST Comparisons

angle	simple cone/flat		cone w/cyl		stage 1 baffle		stage 2 baffle		nested cones	
	visible	LWIR	visible	LWIR	visible	LWIR	visible	LWIR	visible	LWIR
0	4.17E-03	1.08E-03	4.15E-03	1.09E-03	8.61E-05	1.07E-05	5.52E-05	9.77E-06	2.04E-04	1.20E-04
5	3.58E-03	7.09E-04	3.56E-03	6.85E-04	7.63E-05	9.34E-06	4.77E-05	8.83E-06	2.05E-04	1.11E-04
10	2.23E-03	3.03E-04	2.21E-03	2.87E-04	6.91E-05	8.64E-06	4.34E-05	7.71E-06	2.15E-04	1.07E-04
15	1.27E-03	2.08E-04	1.26E-03	1.74E-04	6.05E-05	8.14E-06	4.11E-05	7.08E-06	2.07E-04	1.25E-04
20	8.27E-04	2.16E-04	6.98E-04	1.65E-04	5.36E-05	6.93E-06	3.80E-05	6.13E-06	1.94E-04	1.39E-04

While you could certainly argue that this is an “apples and oranges” comparison, it does serve to illustrate quantitatively how visible and LWIR scatter compare due to different physical processes.

## Comments

- The baffles geometries are simple.. because they are! Fundamentally there are two techniques for controlling scattered light:
  1. Low scatter diffuse coatings
  2. High reflectivity gloss coatings or black mirrors where there is controlled loss and controlled direction
- Certainly “tweaking” is possible but I would not expect to see significant differences relative to these results.
- Particulates are a driver in any low-scatter system, especially in LWIR.
- Adding complexity (i.e., going to a stage 2 baffle) is probably not warranted if it cannot be kept very clean.
- It’s going to take a bit of effort to find BRDF data for black paints in the LWIR. I was able to find some data on several LWIR black paints but not enough to create a valid scatter model. (Publishing scatter measurements of various paints and surface treatments is very much “out of style” these days; most of the scatter data I have is from the 1980’s and early 1990’s. Since so much information is now considered proprietary, the open literature is becoming less useful as a source of information.)