## New Concepts for Inspecting Aspherical Optics

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by

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## Project Objective

- Determine the feasibility of a combined, Hartmann/Digital Holographic interferometry inspection system employing a dynamic holographic optical element.
  - Wide dynamic range for inspecting advanced optical components, including aspheric optics.
  - Complementary measurements with fractional wavelength resolution
  - Measurements with little or no wavefront stitching.

## Key Interests of NASA GSFC

- Primarily reflective optics but also some transmissive
- Mostly visible but some IR
- 100-500mm, larger on rare occasions
- Optics not handled by conventional interferometry
  - Off-axis
  - Conics

- Aspherics
- Toroidal
- Grating blanks

### The Concept



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#### Shack-Hartmann Characteristics



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- Lenslet diameters, d, define spatial resolution over the wavefront being measured.
- δ (sensitivity)
   proportional to *f*, and
   should be less than d
   to prevent confusion

# Constraints in conventional Hartmann Testing that can be obviated with this concept

- Sensitivity requires a longer focal length which can cause focused image overlap of adjacent light pencils.
- If the wave is aberrated, the focused spot will not be round, so its centroid is more difficult to locate, further reducing accuracy
- Spatial resolution is limited to the diameter of the lenses in the array.





#### Data Screen





#### **Control Screen**

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SLM

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Lens

Polarizer\_

Expanded

Laser Beam

Test

Object

CCD

Sensor



#### Scanning Shack-Hartmann System

#### **Control Screen**

#### Data Screen







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### Electronic (Digital) Holography

- Holographic data stored on CCD array.
- Digital wavefront reconstruction
   \* Phase shifting interferometry (hologram plane).
   \* Diffraction theory (propagate to image).
- Interferograms are computed.
- Amenable to fiber optical implementation.

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### Commercial MetroLaser wavefront sensor\*



Object Beam Transmitting Lens

\*Produced by 4D Technologies, Incorporated, Tucson Arizona

### Phase Shifting Interferometry

$$\Delta \phi(\mathbf{x}, y) = \arctan\left(\frac{I_3(\mathbf{x}, y) = I_1(\mathbf{x}, y)}{I_0(\mathbf{x}, y) = I_2(\mathbf{x}, y)}\right)$$

$$\tan(\mathbf{x} - b) = \frac{\tan a - \tan b}{1 + \tan a \tan b}$$

$$\Delta \phi(x, y) = \arctan\left(\frac{\sum_{p,q \in \delta} X(p,q)}{\sum_{p,q \in \delta} Y(p,q)}\right)$$

$$\operatorname{Mask} = \frac{\lambda q}{|b| |a| |k|} + \left(\sum_{p,q \in \delta} \frac{270 \ 90}{|b| |a| |k|}\right)$$

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## Interferogram (one of four)



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#### Wrapped Phase Map of a Test Plate



### Unwrapped Phasemap



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#### Phase Map



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### Modes of Analysis



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# Increasing dynamic range by adjusting the reference wave





- Can preconditioning the wavefront for either Hartmann sensing or extended range interferometry extend the area of coverage in a practical and useful way eliminating stitching?
- How well will a dynamic, computer generated hologram (DCGH), perform the function of wavefront conditioning?

### **Demonstration Breadboard**



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### **Demonstration Breadboard**



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#### Shack-Hartmann scanning a freeform optical component



#### SLM transmissivity



#### Wavefront data

#### Removing wavefront tilt with the SLM



Tilt added to a wavefront



#### Tilt programmed on the SLM

PhaseCam analysis after tilt removal. (Residual fringes due to non linear SLM response.)



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Removing Wavefront Sphere with the SLM



Sphere added to a wavefront



PhaseCam analysis after sphere removal. (Residual fringes due to non linear SLM response.)



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## Key Features and Benefits

- A unique combination enables integrating two powerful, null point, inspection techniques, Hartmann and digital holographic interferometry by using a dynamic holographic optical element.
- Removes existing limitations of Hartman and interferometry.
- Preconditions test wavefront for specific test article, by being programmed to compensate for predicted distortion of a perfectly manufactured part.
- Interferogram recorded and computed by digital holography measures difference between perfect and imperfect optic.
- Electronically Scanned Hartmann sensor measures difference between perfect and imperfect optics focus positions.
- SLM can provide wavefronts of arbitrary shape for testing the measurement system itself, avoiding the problem of unavailability of test items on which to assess the applicability of the inspection system.

### Conclusions

- 1. COTS SLM's are adequate to employ as dynamic HOEs for this concept.
- 2. They require considerable characterization and modification for this application.
- 3. Many waves of tilt and curvature can be compensated by wavefront preconditioning.
- 4. Many limitations of Hartmann testing can be eliminated.
- 5. A combined digital holographic interferometer and an SLM can provide complementary measurements and an unlimited dynamic range.

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#### **NASA SBIR/STTR Technologies**



