

Advanced Mirror Material System

The Peregrine Falcon Corporation Mirror Technology Days SBIR/STTR Workshop 2017

Advanced Mirror Material System

Phase II Objectives

Develop a material system that can...

- Reduce the cost of mirrors by a factor of 4 from current state of the art \$6.5 M/m², while minimizing production time in half.
- Maintain stiffness, low density, stability, and performance.
- Produce mirrors > 4 m in size.
- Match CTE of electroless nickel to Be-38Al substrate by controlling phosphorous content.
- Operate across wide temperature ranges down to low temperature.

Hardware



SEE NOTE 13

R0.016 .015 PLATING ANCHOR

Ø0.38∓.38" .13R MIN. BOTTOM X27 PLACES

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Phase II Effort

- Motivation = Make mirrors more cost effective.
 - $\frac{1}{4}$ cost of James Webb Space Telescope which was \$6.5 million/m²
- When NASA sent men to the moon, no one heard anything about budgets... now everything has to fit into a budget.







Mirrors are Getting Bigger and Bigger



Goal to Make Very Large Mirrors

The bigger the optic, the higher the cost.





Beryllium Significant Substrate Processing

Flowchart I: Beryllium RGA Integrating Structure, Machining Flow Chart







The Process



Mirror Substrate: Be-38AI (LockAlloy)





Be-38Al





Material Comparison Chart of Metals (Ambient Temperature Properties)

Property	Be AMS 7908	Be-38Al AMS 7911	Aluminum 6061 T6	Titanium Ti-6Al4V	Magnesium AZ91D-F
Density (g/cc)	1.85	2.10	2.70	4.43	1.81
Thermal Conductivity (W/mK)	216	210	167	7.8	72.7
CTE (ppm/°C)	11.4	13.9	22.9	9.0	26
Modulus of Elasticity (GPA)	303	192	69	110	45
Ductility (%)	2	2	8	10	3
Yield Strength (MPA)	241	192	255	1034	150
PEL (MPa)	>30	17.3	<6.5	N/A	NA
Specific Heat (J/kg°K)	1925	1506	896	597	NA
Electrical Conductivity (% IACS)	41	45	43	N/A	<40
Melting Point (°C)	1285	1082	652	1660	650
Specific Stiffness	164	91	26	25	25

Mirror Surface: Electroless Nickel





In Phase I, we demonstrated a phosphorous match.

Influences on the As-Plated Nickel Deposition Residual Stress

- Bath Chemistry (Including P%)
- pH
- Temperature
- Agitation

• MTO (Metal Turn Over; small amount of solution drained of (~1%); solutions added)

- The bath age
 - Fresh Bath; deposition layer tends to have residual stresses that are in compression (~5,000 psi).
 - Baths with 3 MTO; depositions tend to be stress free (use in line controller to maintain MTO 3 bath).
 - Baths with over 3 MTO; depositions tend to have residual stresses that are in tension (~3,500 psi).

Electroless Nickel



The sample to the left is cut in half and the cross section polished. The view to the right shows the cross-section and the X-ray beam scan line

Electroless Nickel





X-Ray Analysis of the Cross Section of EN Plating

X-Ray Analysis of Spot 2 on Sample A-1

Qualitative Elemental Analysis (Preliminary)								
Element Number	Element Symbol	Element Name	Weight Concentration	Error				
28	Ni	Nickel	88.6	0.0				
15	Р	Phosphorous	11.4	0.0				

X-Ray Fluorescent Microscopy



Curtesy Georgia Tech

Through the Thickness Elemental Composition of a Peregrine Sample (10 keV Beam, 300 nm Size)

X-ray Microfluorescence



Variations of P & S elements concentration through the thickness of a sample 100 μm coating

Demonstrates the "Power of Technique"

Through the Thickness Elemental Composition of a Peregrine Sample



Variations of Ni concentration through the thickness of a sample 100 μ m coating

Allowable Stress

Achieving a "stress free" substrate then:

Max allowable range of stress in the system (compressive or tensile) $\,\sigma_{max}$

Thermal expansion and Youngs modulus of substrate

Thermal expansion and Youngs modulus of plating

Temperature of the bath

Lets define residual stress $\sigma_{\rm r}$

 $\sigma_{\rm r} = \int_{T_{bath}}^{T} [E_{\rm s}\alpha_{\rm s}({\rm T}') - E_{\rm p}\alpha_{\rm p}({\rm T}')]d{\rm T}'\}$

where the integration limit T is any temperature in the operating range at which σ_r has a maximum (tensile) or minimum (compression)

 $\alpha_{s}(T), E_{s}(T)$ $\alpha_{p}(T), E_{p}(T),$ T_{bath}

Manage the Bath to Minimize Residual Stress



Joining: Liquid Interface Diffusion Bonding



Parts Joined Together under Temperature and Pressure



Liquid Interface Diffusion Bonding

Enables large mirror production.



Stage 1



Stage 2



Stage 3



The major stages in LID Bonding...

1. Preplacement and fixturing of parts

- 2. A liquid front smooths the interfaces
- 3. The intermediate layer diffuses into the base metal
- 4. Diffusion occurs to create a homogeneous joint

Mirror Surface: Single Point Diamond Turning



Integrated Test: 90 mm Mirrors



Both the monolithic and segmented mirrors were processed through electroless nickel side by side. Only thing that is different in the second one is that it was liquid interface diffusion bonded together.

Monolithic Mirrors



Monolithic Mirrors – Baseline



Monolithic Mirrors – After Thermal Cycling



- Showed little movement from baseline to thermally cycled mirrors.
- These mirrors are very stable over long periods of time.
- Everything is somewhat unstable; it degrades at some level over time.
- Goal would be to have the system operate over a wide temperature range.
- We want a usable system that is cost effective.

Segmented Mirrors

Manufacturing Flow Chart

(Major Steps for LID Bonded Mirrors)



Segmented Mirrors – Baseline



Segmented Mirrors – After Thermal Cycling



The LID bonded, segmented mirror produced more stability than the monolithic mirror. It was able to withstand higher temperatures over longer periods of time.

Integrated Polish



Because of its success, we want better resolution on movements through the use of re-polishing the optics to get to an even finer finish before we retest them.

This should yield even better results.

Test Data – 90 mm Polished Monolithic Mirrors

















Cycled to -60°C

Test Data – 90 mm Polished Segmented Mirrors



Cycled to 0°C

Cycled to -60°C



Cycled to -20°C

Cycled to -72°C



Cycled to -40°C





¹/₂ m Sized Optics





Initial Monolithic ¹/₂ m Design based on JWST Mirrors

¹/₂ m Sized Optics



Deflection at 10g Loading



Equivalent Weight Designs, The Closed Back Be-38Al Design is Equal to Weight and Stiffness to the Beryllium Design on the Left



Various Design Scenarios were Explored

Monolithic Mirrors



1/2 m Optic – Monolithic Mirror

BASELINE





AFTER ALL THERMAL CYCLING

Segmented Mirrors



¹/₂ m Optic – Segmented Mirrors



BASELINE

AFTER THERMAL CYCLING AT LOW TEMPS.



Hardware (1/2 m Mirrors)













Advanced Mirror Material System

PI Robert Hardesty



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Be-38A1 / LID Bonding / Electroless Nickel Plating (CTE Matching) / SPDT- Polished

Testing demonstrates stability to $1/50^{\text{th}} \lambda$





Future Planned Developments

Planned Post Phase II Partners

Peregrine has the ability to produce mirrors using this technology – however, we seek Partnerships on a program by program basis.

Planned / Possible Mission Infusion

- 1. CIBER-2 a Sounding Rocket Telescope application for 80K operation.
- 2. Visible to MWIR Imaging System for Military application.

Planned / Possible Commercialization

After initial key applications development, we plan to pursure scan mirrors and Earth Observation Athermal Systems.

Accomplishments

- Matched (WI +/- .2%P) Electroless Nickel (EN) Plating to Be-38Al to yield a stable substrate.
- Seamlessly joined Be-38Al together that can create large substrates for mirrors (no surface indication).
- Demonstrated stability to $1/50^{\text{th}} \lambda$.
- Successfully tested across large temperature ranges down to low temperatures.
- Delivered two half meter mirrors (Monolithic and LID bonded versions) using SPDT at an areal cost of <<\$1M/m².

Key Milestones Met:

- Dialed in Electroless Nickel Plating process to +/-.2%P.
- Dialed in Liquid Interface Diffusion Bonding process for seamless joints.
- Integrated Be-38A1/LID Bond/EN/SPDT to create stable substrates.
- Tested Material System over wide temperature range to low temperatures.