

Lightweight, Scalable Manufacturing of Telescope Optics

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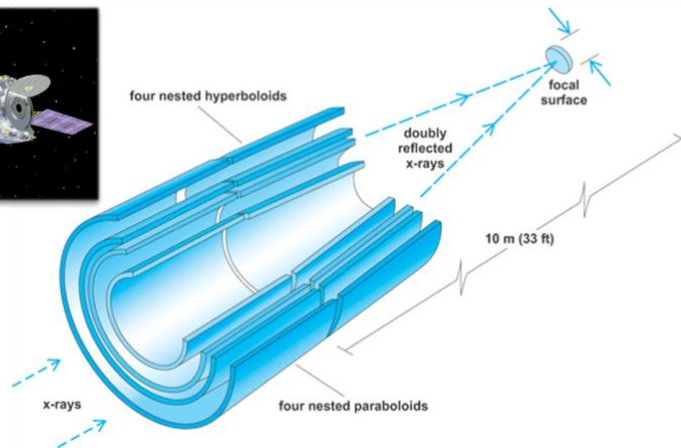
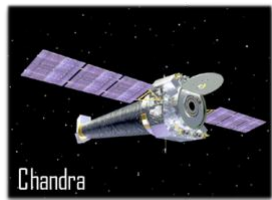
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Need for Lightweight Telescope Optics

- Decrease the weight of current Wolter Type I optics to allow for greater shell packing and thus increase effective X-ray collection area (i.e. increase the optical surface area per unit mass)
- Reduce the requirements and cost of telescope launch vehicle

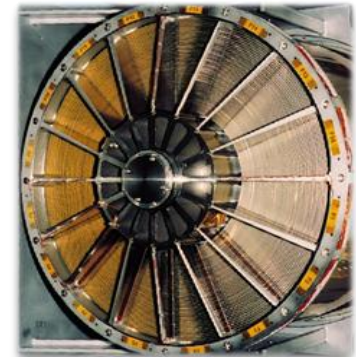


Chandra X-ray observatory utilizing 4 nested zerodur optics with the outer shell measuring 1.2 meters in diameter.

Cross sectional view of Wolter I optic showing grazing angle reflection and nested reflector capability



XMM Newton



Current State of the Art X-ray observatory (XMM Newton) utilizing 58 nested reflector shells; largest reflector 70cm diameter.

Note the increased number of shells compared to that of Chandra resulting in greater optical area and thus greater X-ray collection

Benefit of Electroformed Optic

- Individual mirror thickness reduced by greater than an order of magnitude (1mm vs. 20mm)
- Reduced mirror thickness allow for a greater number of shells to be nested

Disadvantage of Electroformed Optic

- Density of Ni compared to zerodur
- Figure accuracy not as good as zerodur

Electroformed nickel replication (ENR)

Repeat



Benefit of the Electroforming Process

- Well suited for precision replication (widely used in optical manufacturing)
- Superpolished mandrel is reuseable, can be “touched up” as necessary

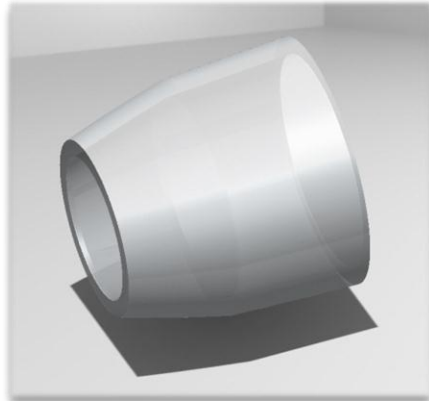
Disadvantage of Electroformed Optic

- Density of Ni compared to zerodur (8.9g/cm^3 vs 2.5g/cm^3)
- Figure accuracy not as good as zerodur

NiCo alone is too heavy for X-ray telescope missions

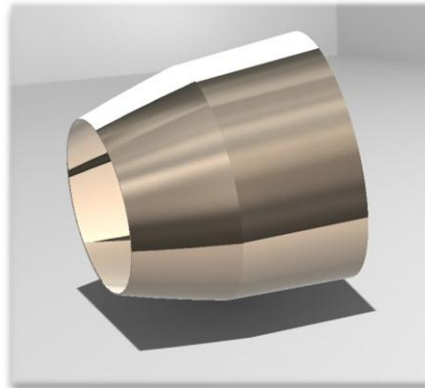
There exists a need to replace much of the NiCo with a less dense material

Current Standard



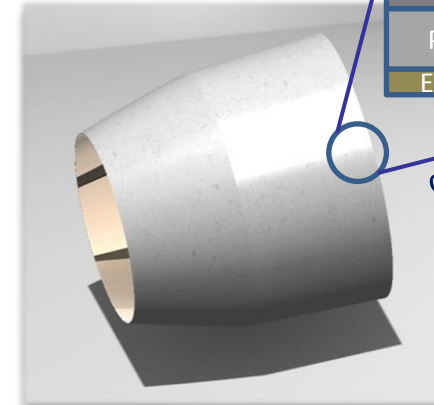
20mm Zerodur

Current State of the Art



1mm NiCo

Proposed Innovation



$\leq 100\mu\text{m}$ NiCo
 $200\mu\text{m}$ Al_2O_3

Dense $\text{Al}/\text{Al}_2\text{O}_3$

Porous $\text{Al}/\text{Al}_2\text{O}_3$

Electroformed Ni

cross section

Thickness of NiCo remains constant as shell diameter increases

Comparison : Mass of Wolter I Optic with a 70cm diameter, 60cm long

68.7 kg

11.8 kg

1.9 kg

Proposed Innovation

- Replace zerodur optic with NiCo shell and thermal spray ceramic support structure
- Utilize NiCo electroforming to replicate the surface micro-roughness of the mandrel
- Combine a graded-density lightweight ceramic support coating to hold figure accuracy and supply rigidity for handling



Thermal Spray Processes

Twin Wire
Arc

Flame /
Combustion

Atmospheric
Plasma Spray

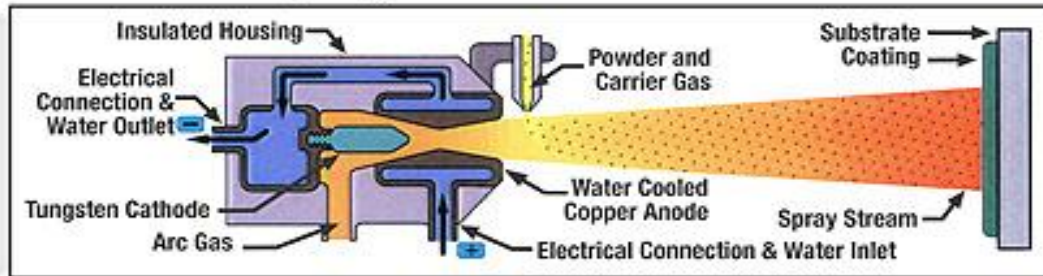
High Velocity
Oxy Fuel

Cold
Spray

Detonation
Spray

Plasma Spray Process

Associated
with more
than 100
variables



http://www.thermalspray.org/site_plasmaarc.asp

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Characteristics

Flame Temperature:
Approximately 12,000 - 20,000°F
(6,000 - 11,100°C)

Gases Used:
Ar/H₂
N₂/H₂

Particle Speed:
800 - 1,800 ft/s (240-550 m/s)

Photo Courtesy of Westaim Ambeon

Spray Conditions:

- Torch Settings
- Powder
- Substrate Condition
- Spray Pattern

In Flight Particles:

- Temperature
- Velocity
- Trajectory

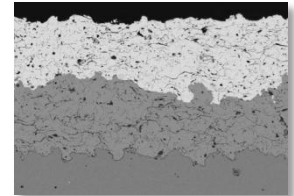


Coating Build-up:





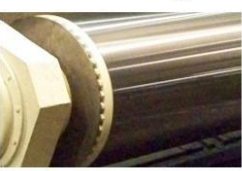
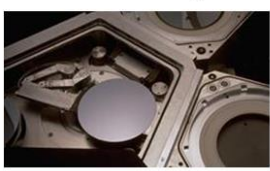






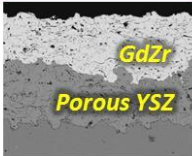
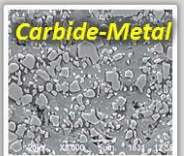
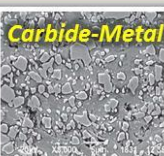
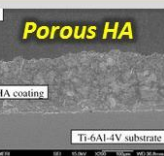
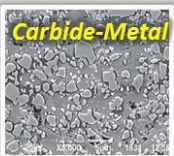
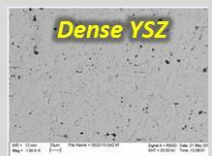
- Splat Morphology
- Microstructure
- Porosity
- Interlamellar Contact

Properties:

- Mechanical
- Thermal
- Reliability



Wide Range of Thermal Spray Coated Components

APPLICATIONS	Energy - Gas Turbine Engine 	Industrial machinery 	Aviation Engine / Landing Gear 	Bio-implants 	Metal / Paper Manufacturing 	Electronics Manufacturing 
Thermal Spray Processes						
COATING MATERIAL & MICROSTRUCTURE						
PHYSICAL CHARACTERISTICS	Thickness Weight Porosity	Thickness Crack Porosity	Thickness Crack Weight	Thickness Defect Density Roughness	Thickness Crack Roughness	Thickness Defect Density
PROPERTIES & PERFORMANCES	Residual Stress Adhesion Sintering/Aging Conductivity Toughness	Residual Stress Adhesion Strength Toughness Wear	Residual Stress Adhesion Strength Toughness Wear	Residual Stress Adhesion Toughness Phase Stability	Residual Stress Adhesion Strength Toughness Wear	Residual Stress Adhesion Erosion Phase Stability Thermal Expansion

Materials Selection

- Wide array of materials to select from
 - Metals, ceramics, polymers, composites
- Ability to tailor the material to not only match the expansion but also provide compliance via defects (thermal cycling compliance)

Process Parameters

- Ability to tailor the microstructure, density, and interface through use of graded layers
- Ability to control deposition temperature
 - Robot raster speed
 - Secondary cooling

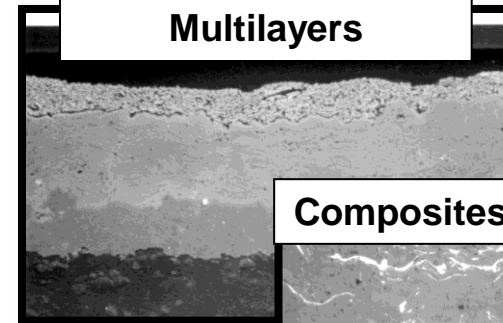


NiAl deposited onto canvas

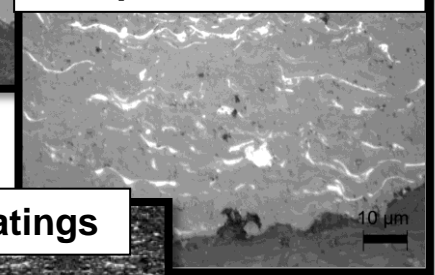
Component Manufacturing

- Ability to deposit onto large cylindrical geometries
 - Easily scalable
 - Deposit directly onto electroformed shell
- Cost effective and efficient
- Established industry base, does not require large capital expense for application

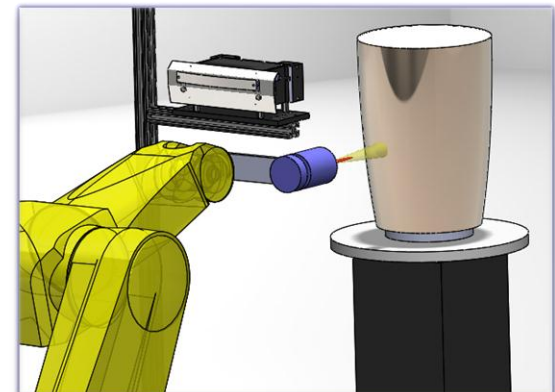
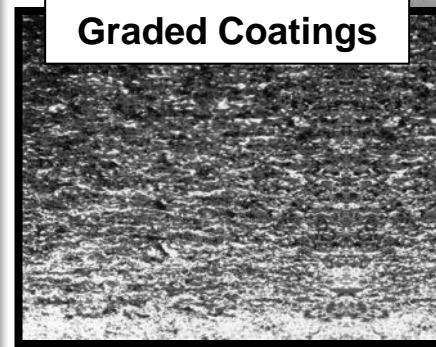
Multilayers

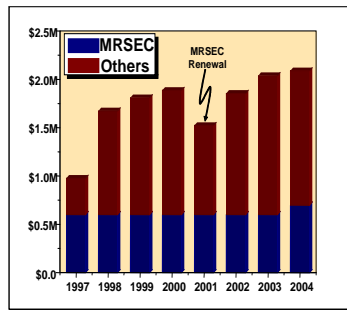


Composites/Cermets



Graded Coatings





Value Added Benefits from Core NSF Funding



Consortium is operated by the Center for Thermal Spray Research at Stony Brook University



Advanced tools, software, and technology services company



Expanded to new location Summer 2012

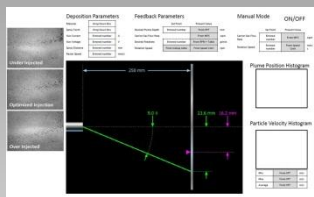
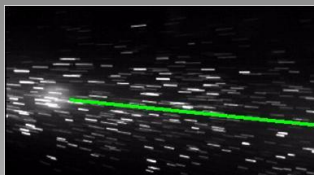
ReliaCoat Technologies *Founded May 2009*



Advanced Hardware & Software Technologies

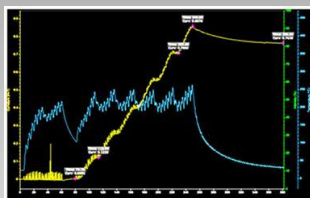
Linking Advanced Science
to Industrial Products

Injection Monitoring & Feedback



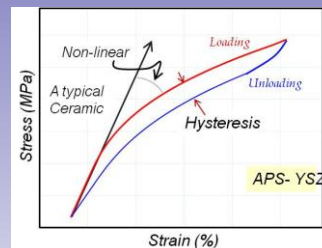
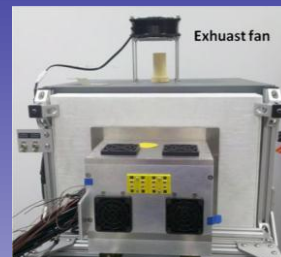
- Injection depth measurement
- Closed-loop carrier gas flow control
- Closed-loop feed rate control

In-Situ Coating Property Sensor



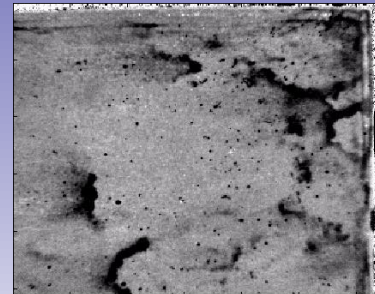
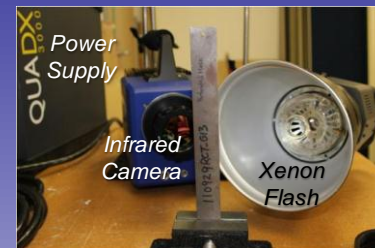
- In-situ residual stress evolution
- Elastic modulus
- Monitoring coating build-up

High Temp Ex-Situ Coating Property



- High temperature coating compliance
- Nonlinear anelastic behavior
- Thermo-cyclic residual stress evolution

NDE: Flash Imaging Tomography



- Non-destructive, non-invasive coating structure assessment
- Coating crack & delamination detection

Material Compatibility

- Thermal mismatch

Minimal Coating Residual Stress

- Separated optic shape retention

Coating Adhesion

- Bond strength

Minimize Thermal Input to Mandrel

- Figure accuracy

No Damage from Particle Impact

- Optical surface distortion

Environmental Considerations

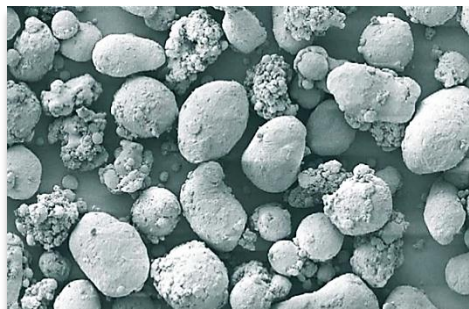
- Vacuum
- Outgassing



**Prototype Multilayer
Coated Electroformed
Hard X-ray Telescope**
(NASA/MSFC and Brera Obs.)

Defined Challenges	Proposed Mitigation Strategies
Light weight, rigid & high toughness carrier layer	<ul style="list-style-type: none">▪ Base structure of Al₂O₃ or other porous ceramic coating▪ Al₂O₃-Aluminum composite/functionally graded structure





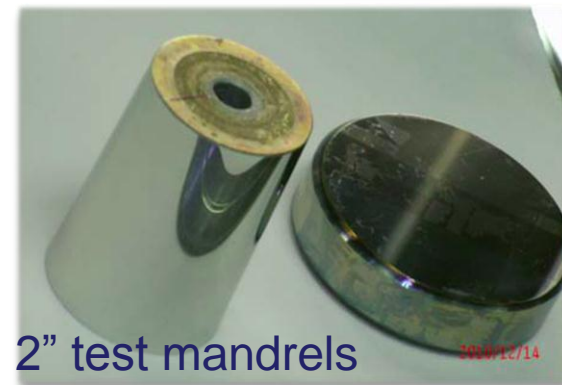
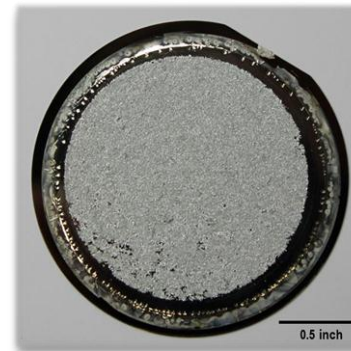
Aluminum Powder

Fine powder size to minimize particle energy

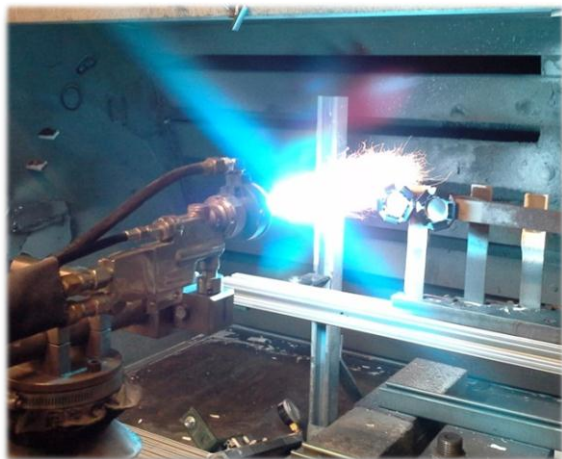
Initial Test Substrates



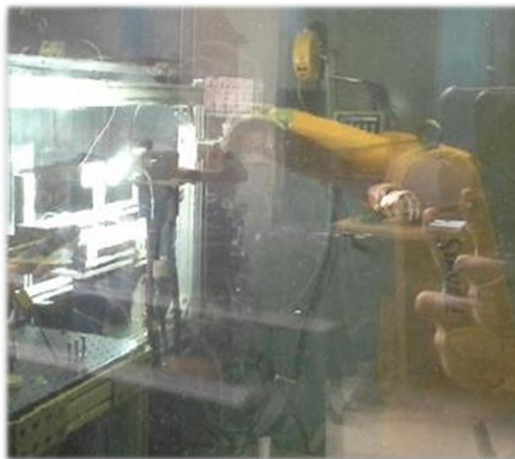
Evaluate potential particle damage using nickel and aluminum foil



2" test mandrels



Flame Spray



Plasma Spray

Process development using NiCo plated silicon wafers (due to mandrel availability), continued testing on flat and conical mandrels to evaluate X-ray performance



X-ray reflectivity measurements