

Thermal Stability Design, Analysis and Verification of a Starshade

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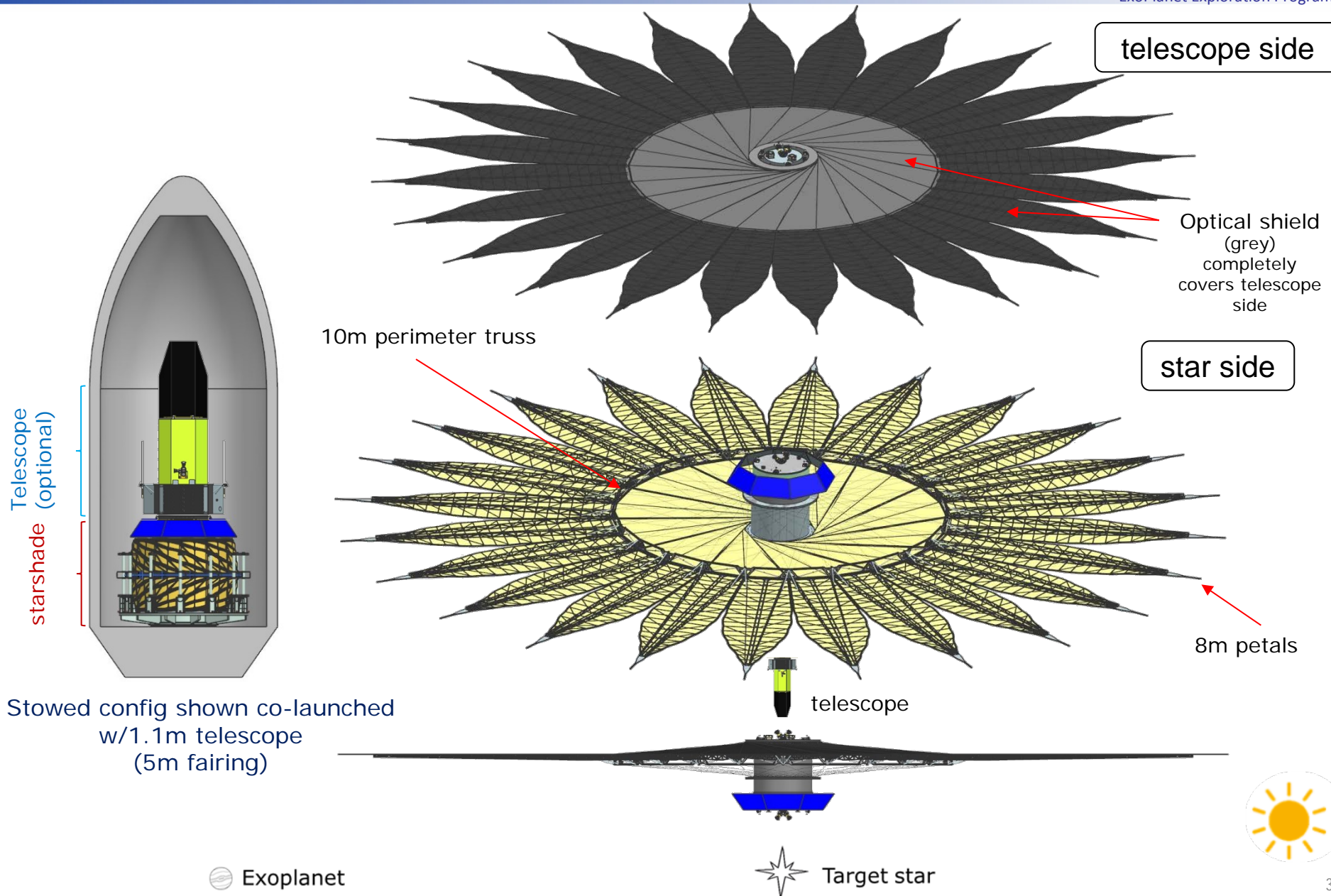
Agenda

- Starshade design overview
- Thermal analysis overview
- Distortion analysis
- Monte Carlo analysis
- Testing and verification

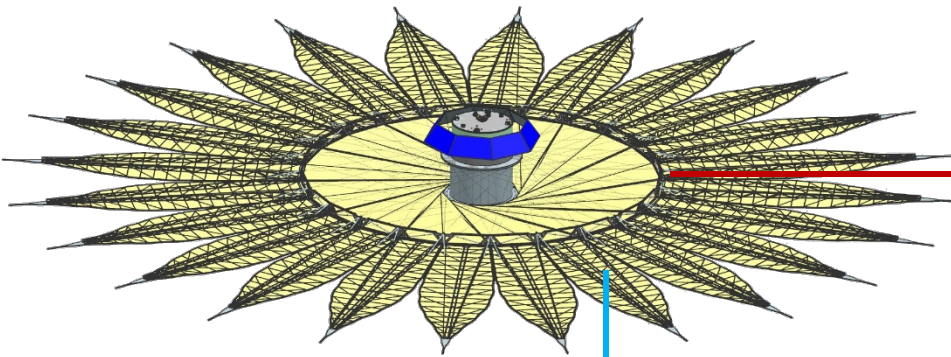
Starshade Design

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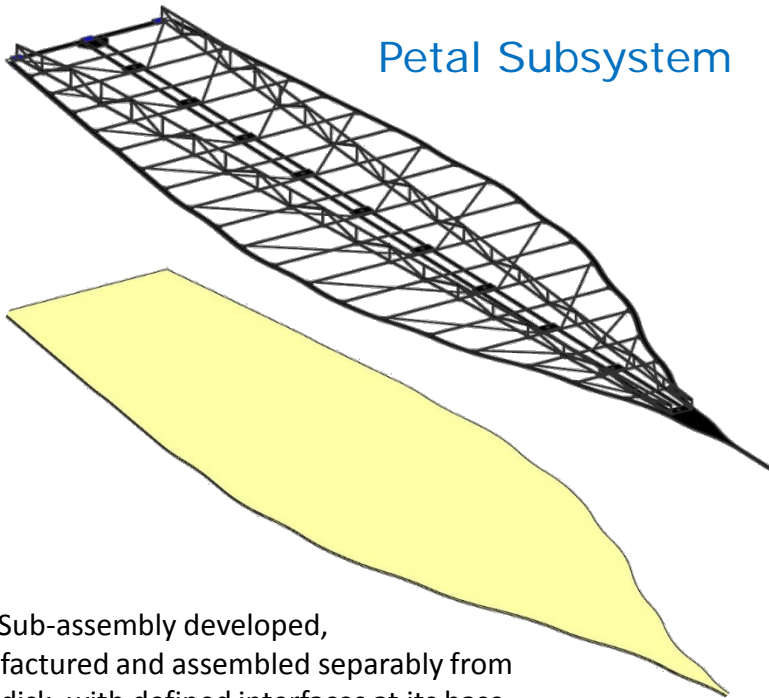
26m NI2 design with 8m petals for ExEP Architecture Trade Study



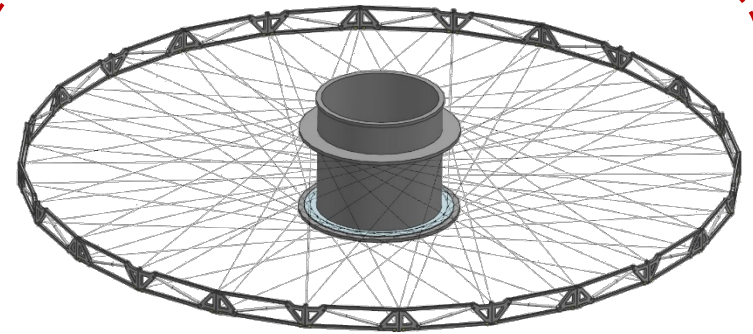
Subsystem Definitions



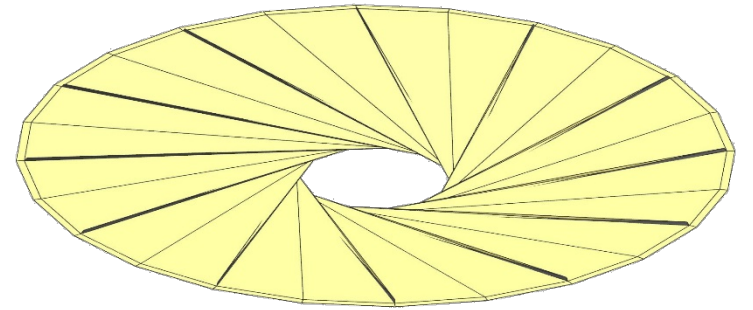
Petal Subsystem



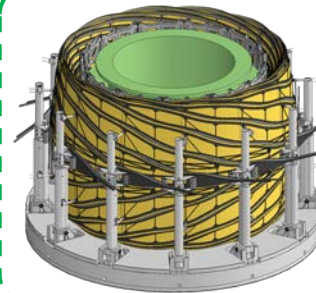
Petal Sub-assembly developed, manufactured and assembled separably from inner disk, with defined interfaces at its base



Truss + spokes + hub constitute separable structure w/defined interfaces to petal



Inner Disk Subsystem

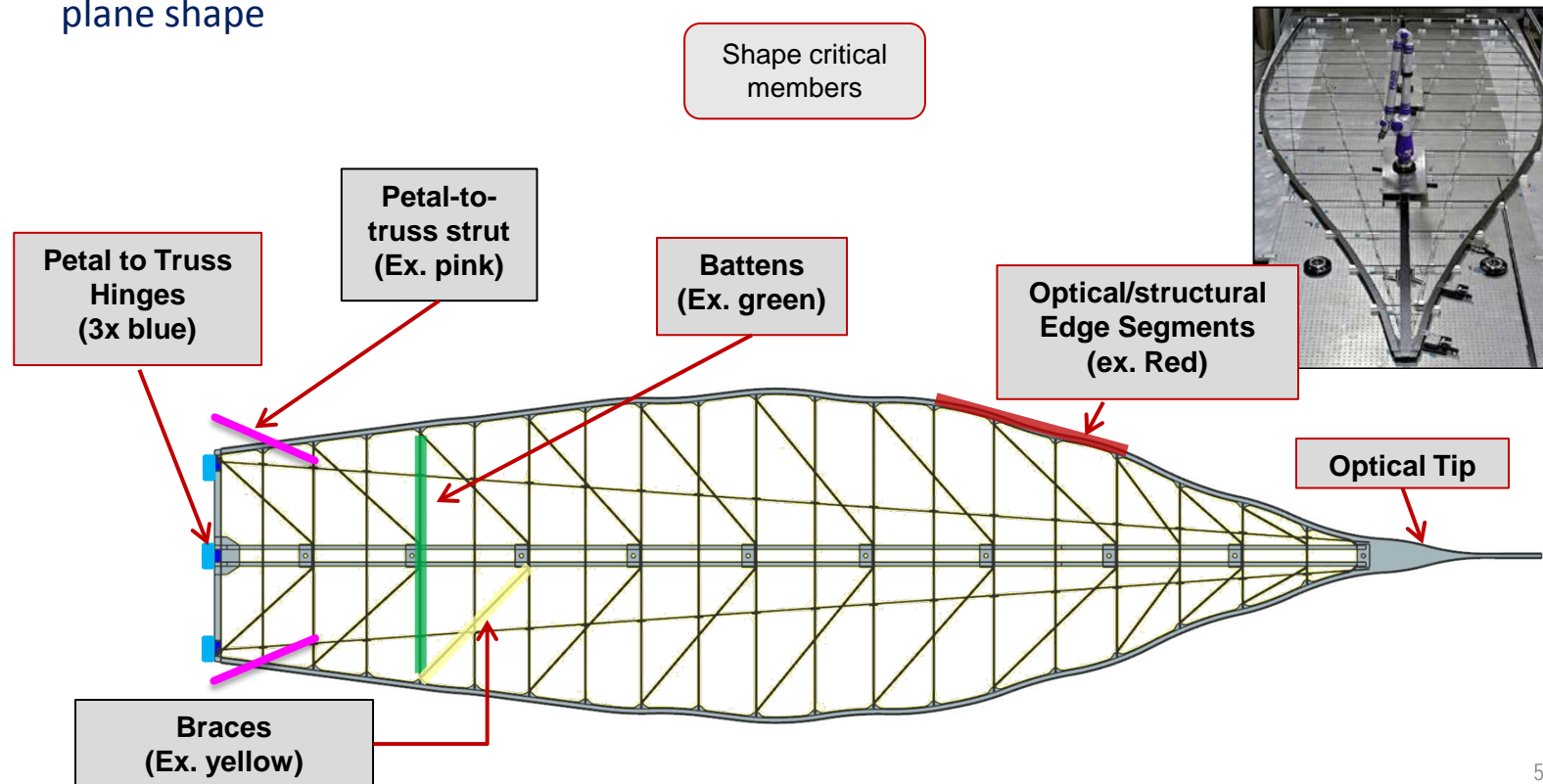


Petal Launch Restraint & Unfurl Subsystem (PLUS)

PLUS controls petal deployment & defines petal L/R interfaces (jettisoned after launch)

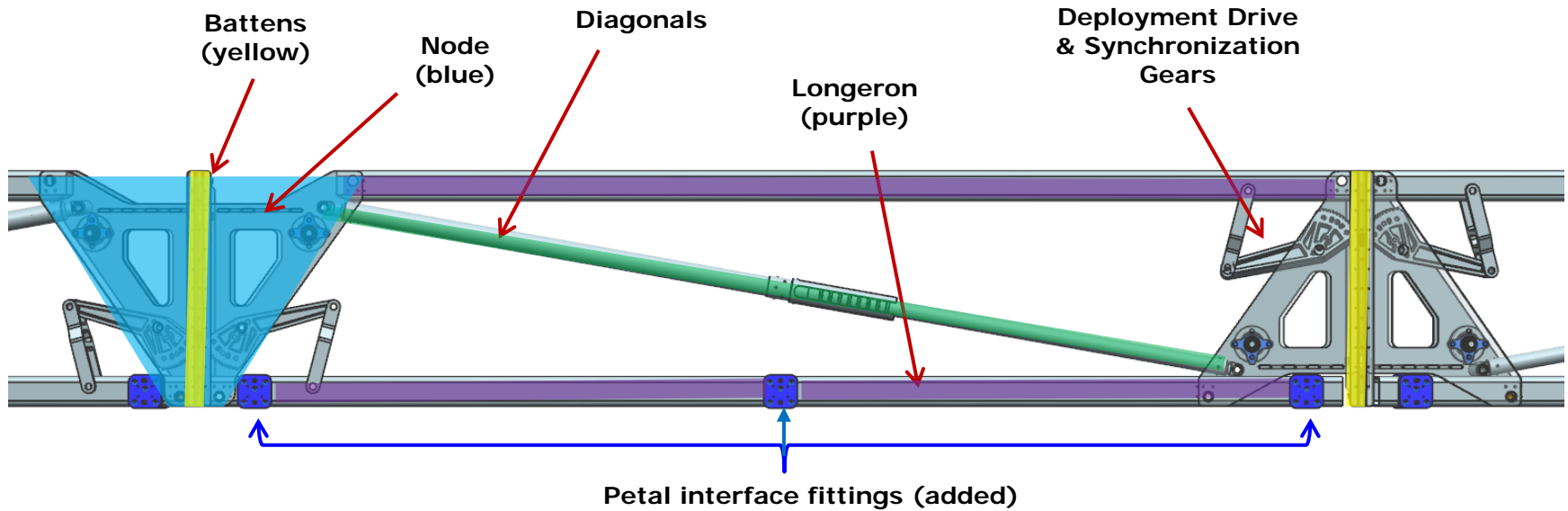
Petal Shape Critical Components

- Petal designed specifically to address in-plane shape stability
 - Battens maintain petal width (COTS & precise)
 - Edges are width-wise thin and “go where battens tell it to”
 - Braces (diagonals) provide in-plane shear stiffness to maintain shape
- Petal hinges maintain petal position relative to truss (w/std avail. precision)
- Petal-to-truss struts provide out-of-plane support & must minimally influence in-plane shape



Inner Disk Design Basis (Perimeter Truss)

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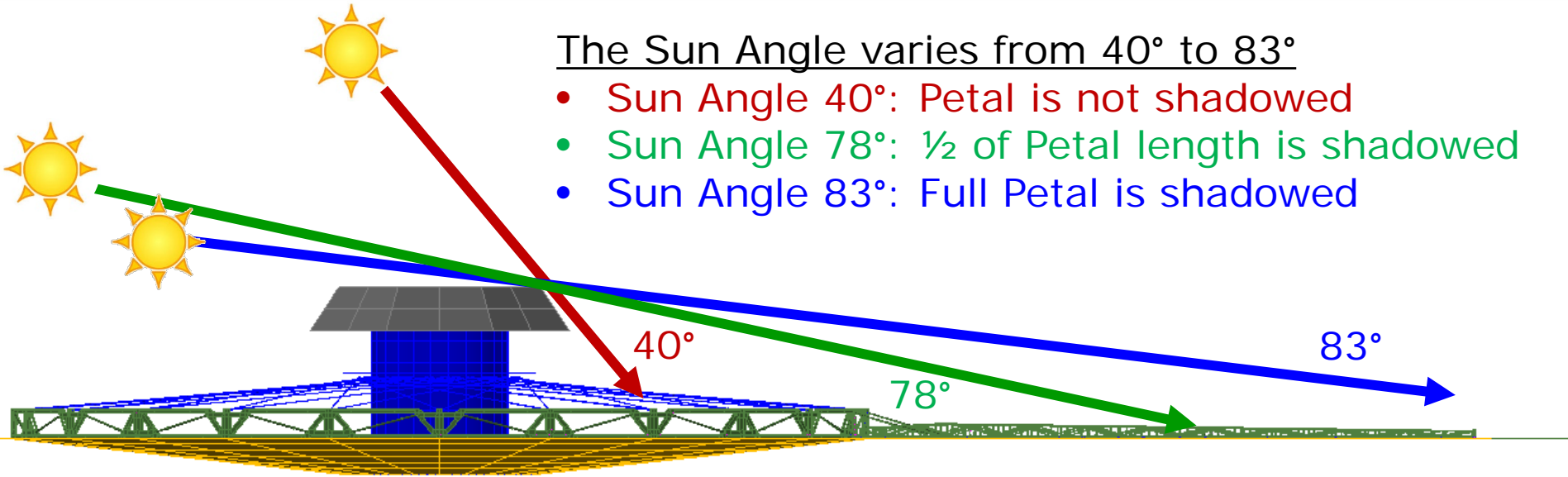


Sun Angles and Shadowing by Hub

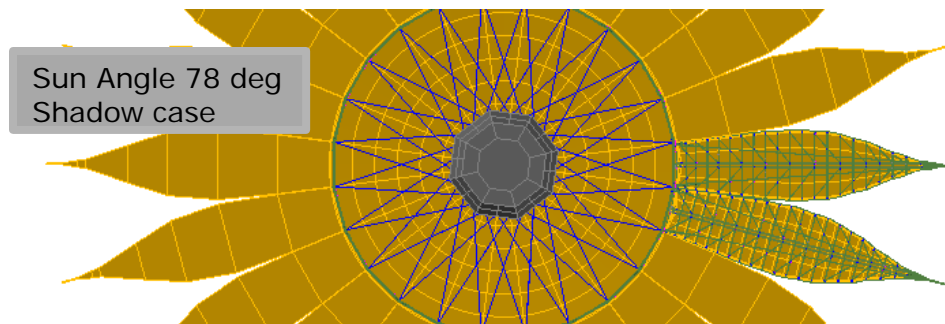
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The Sun Angle varies from 40° to 83°

- Sun Angle 40°: Petal is not shadowed
- Sun Angle 78°: ½ of Petal length is shadowed
- Sun Angle 83°: Full Petal is shadowed

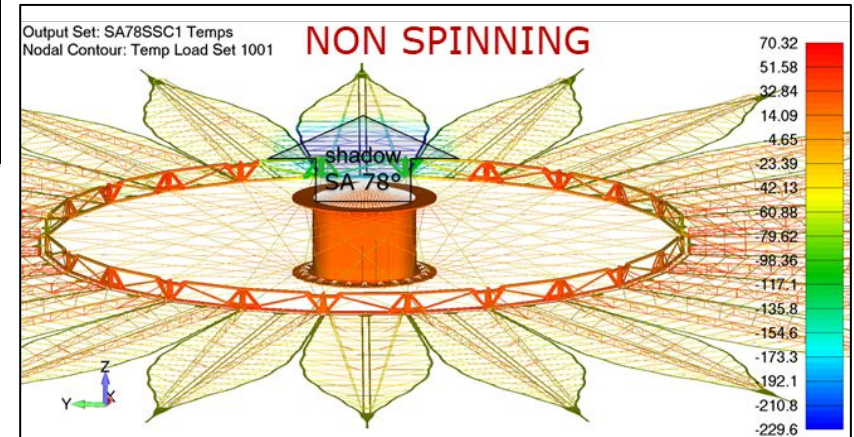
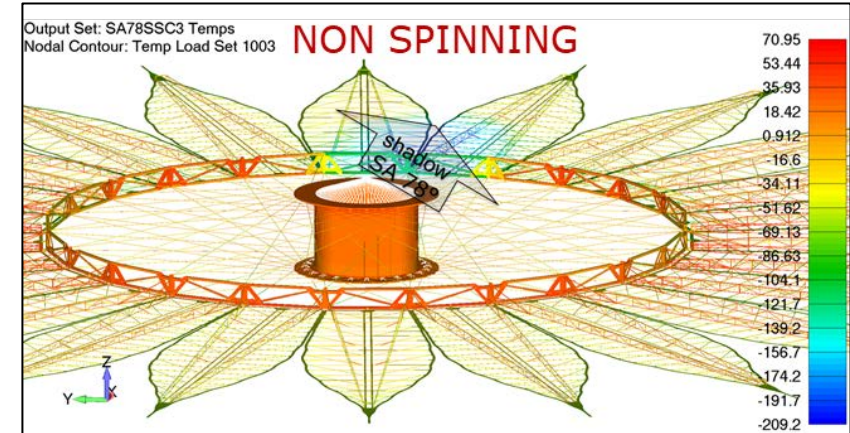
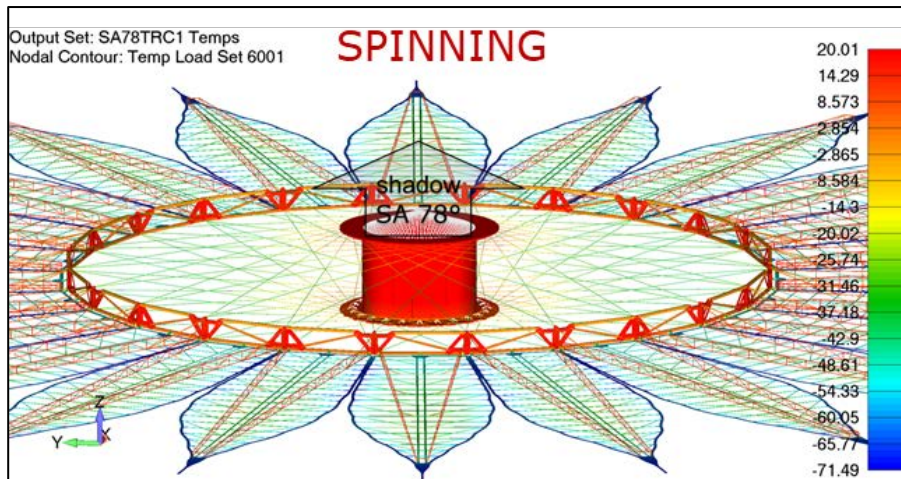


*** Slow rotation run every 3.75°. @1/3 RPM this is every 1.875 seconds, 96 positions. Temperatures available at each of the 96 locations.



Non-spinning Shadow Orientation Conclusions

	Comment	Gradient	Max/Min Temp
NON-Spinning	Shadow clocking orientation has little effect on max/min temps, only moves cold portion of starshade	300 C	70 C / -230 C
Spinning	Averages temperatures symetrically around spin axis Transient has negligible effect on contrast	90 C	65 C / -95 C



Sun Angle 78

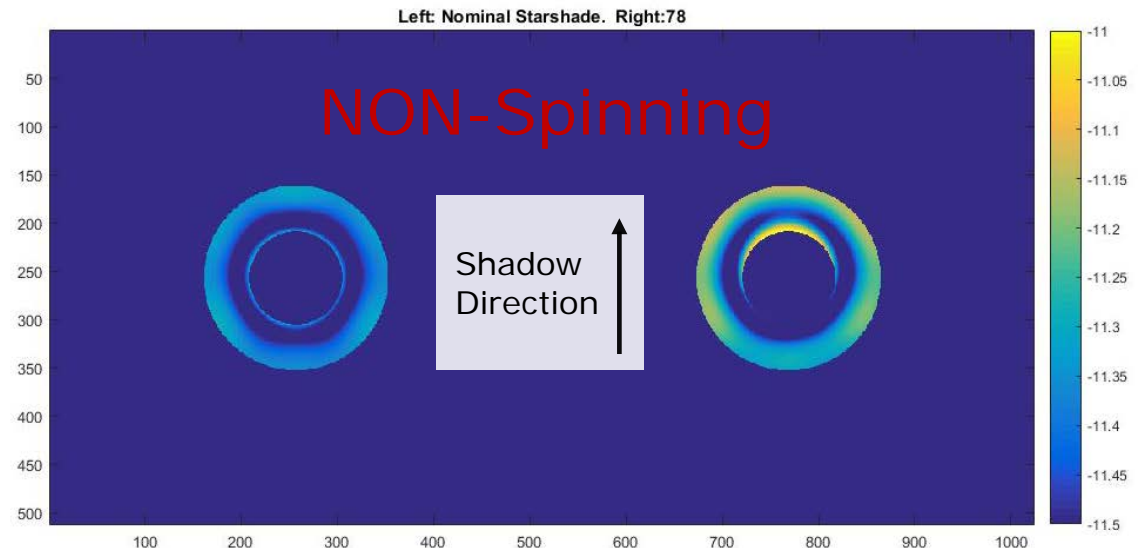
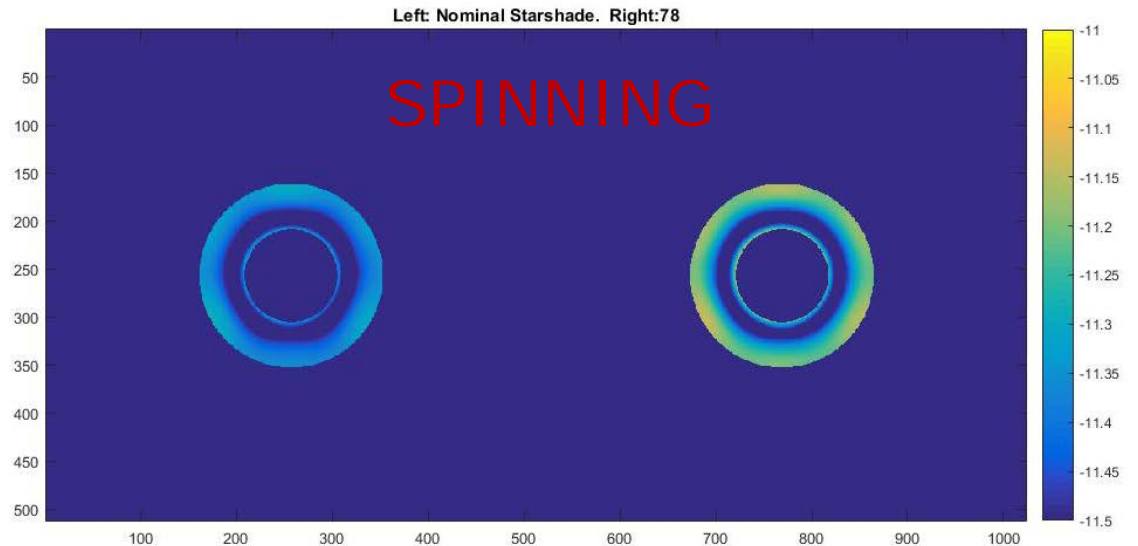
Comparison of Spinning to Non-Spinning

Spinning

- Spinning has a telescope axis-symmetric contrast
- Contrast varies radially

NON-Spinning

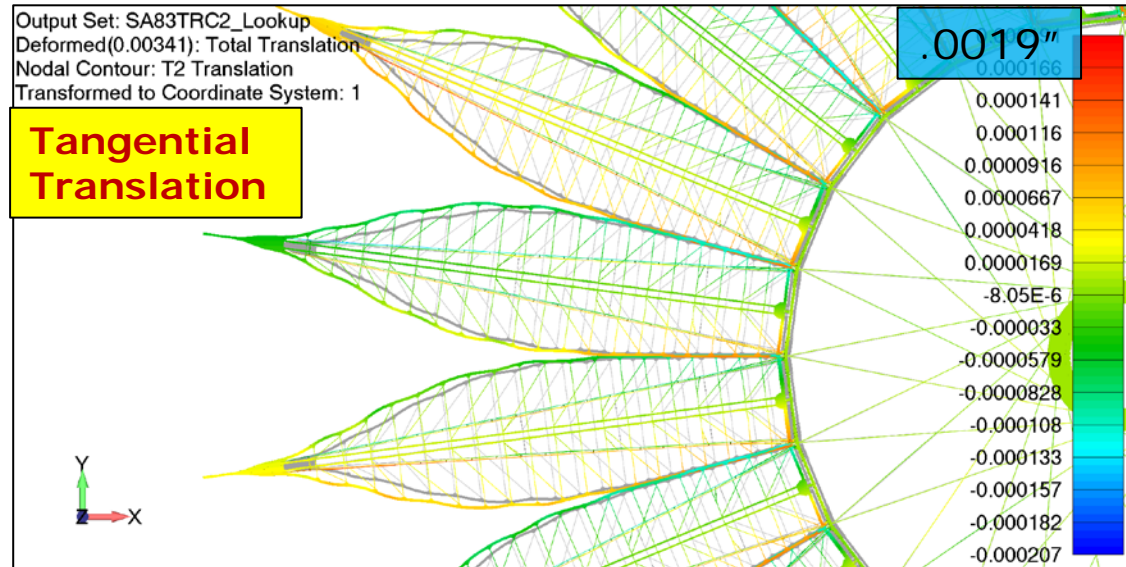
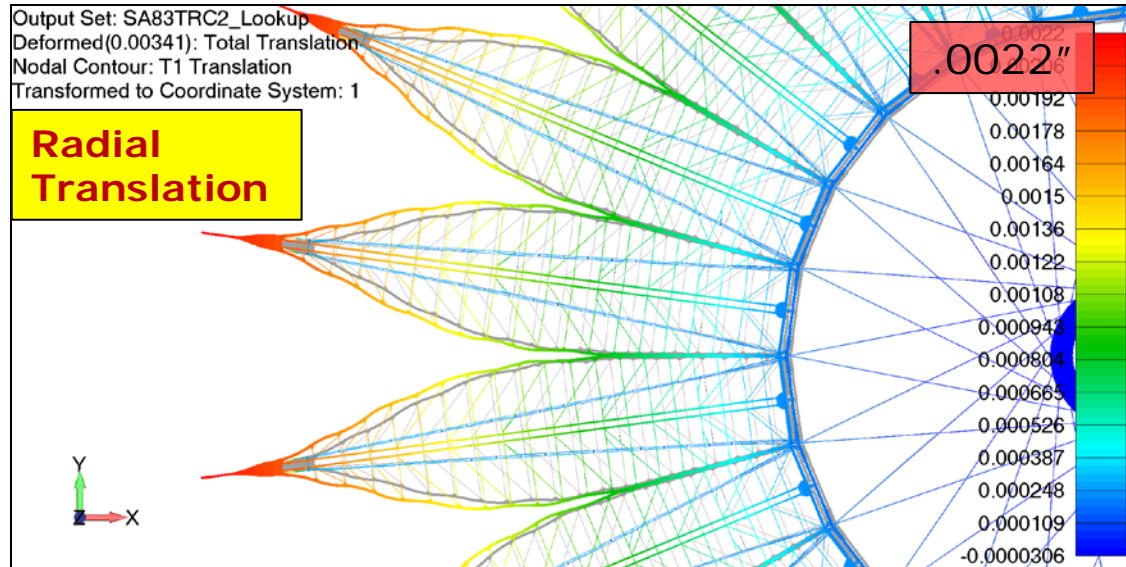
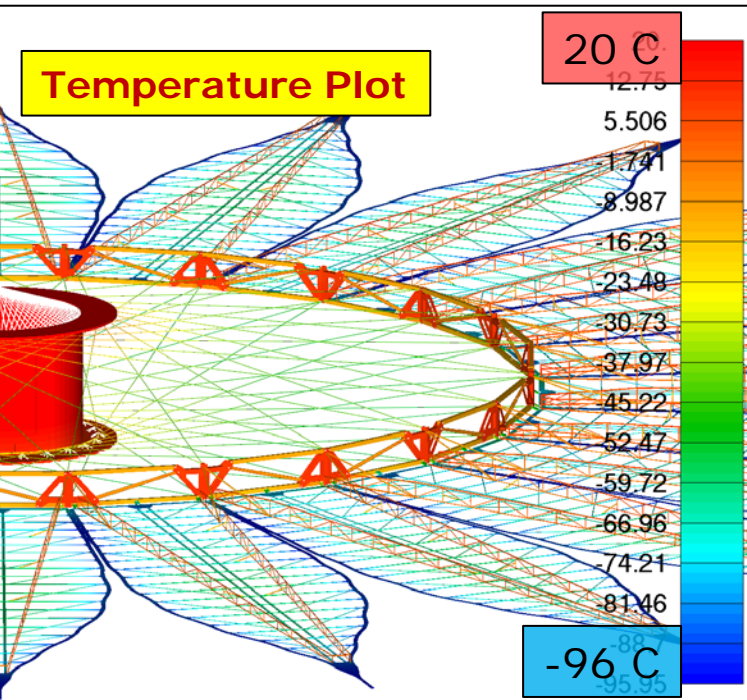
- Largely distorted shadowed petals :
 - Shift high contrast annulus toward shadow
 - Reduce contrast in petal distorted zone



SA83 SPINNING Distortions

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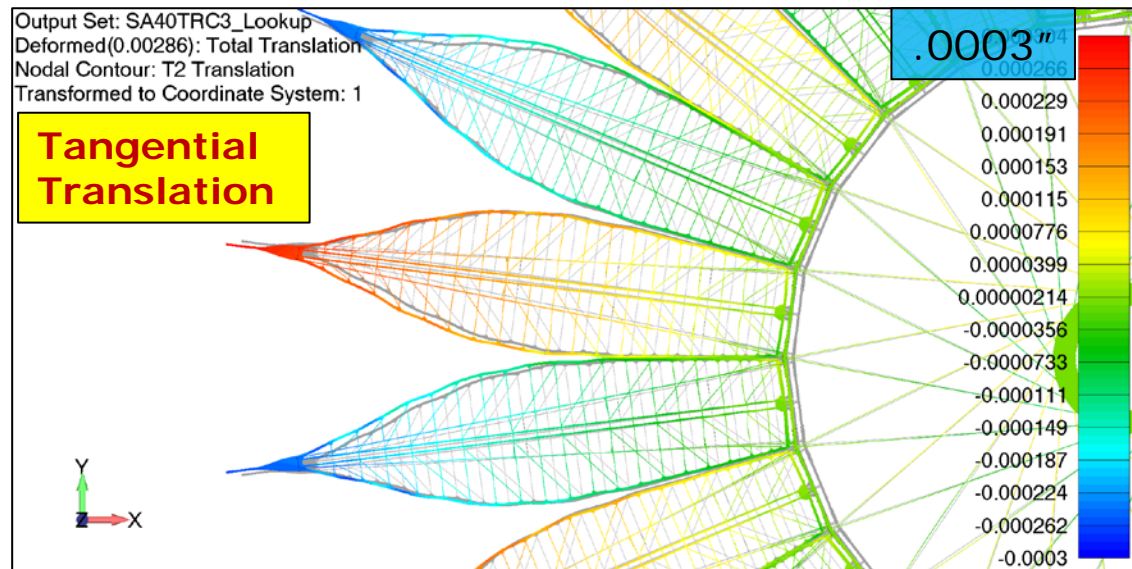
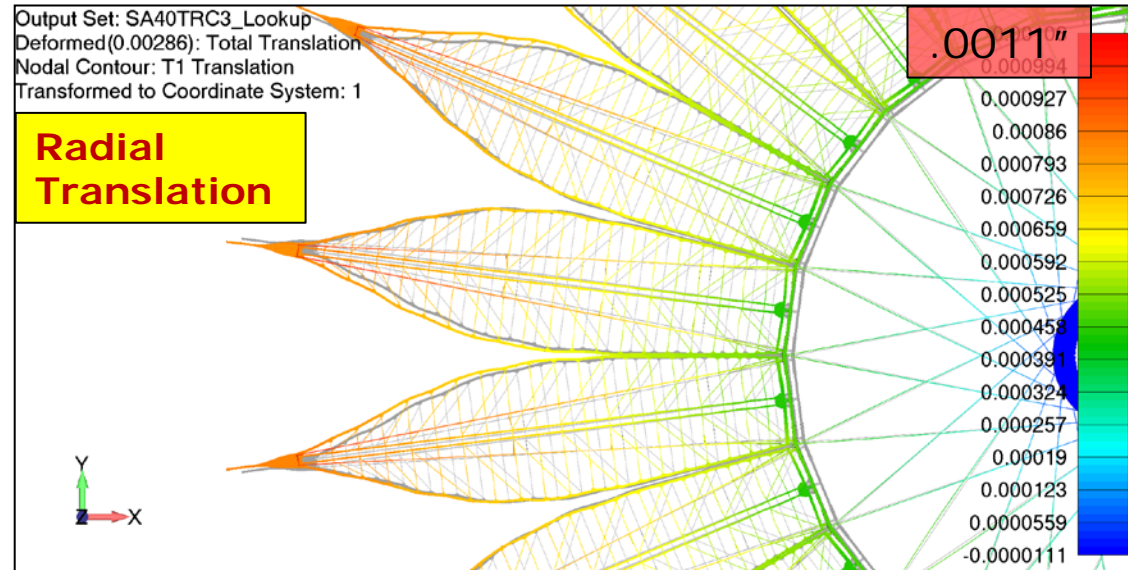
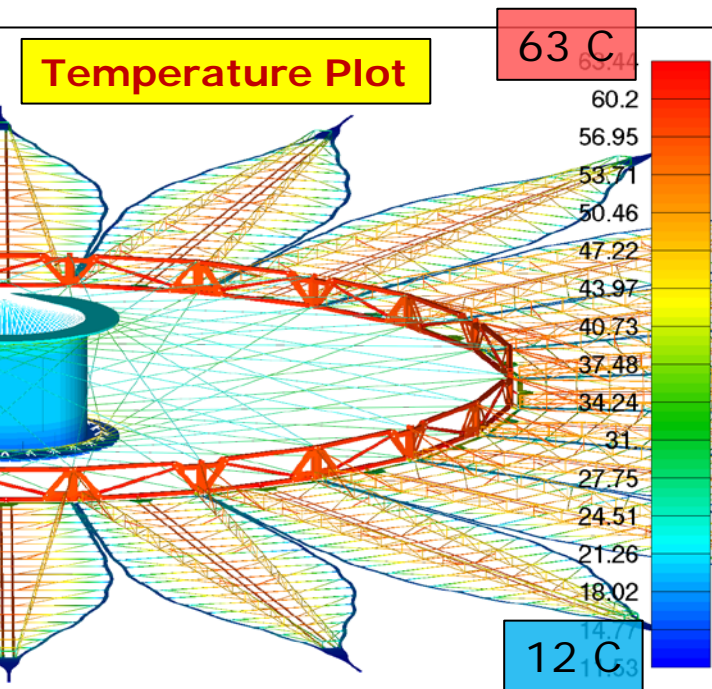
- Raw distortions on order of 50 microns (0.002")
- Distortions correspond to temperature results (thermal analysis), e.g.
 - Truss @ 20 C (room temp) = almost no shape change
 - Petal dT = -65 C, 50 microns (0.002")



SA40 SPINNING Distortions

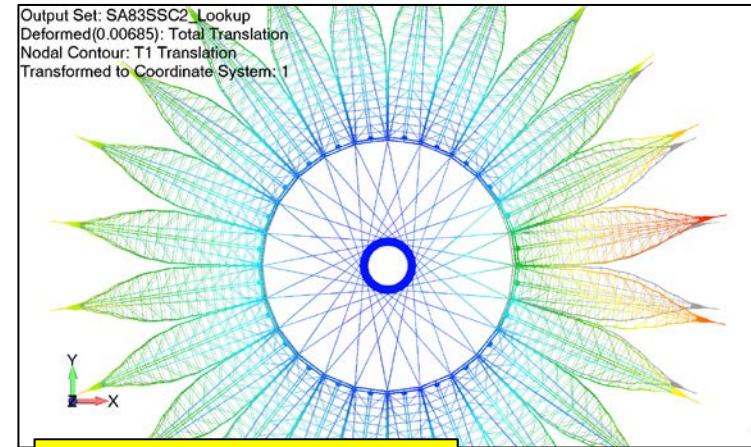
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- Raw distortions on order of 50 microns (0.001")
- Distortions correspond to temperature results (thermal analysis), e.g.
 - Truss @ 60 C (dT = 40C), ~25 micron radial expansion
 - Petal dT = ~+40 C, 30 microns (0.002")



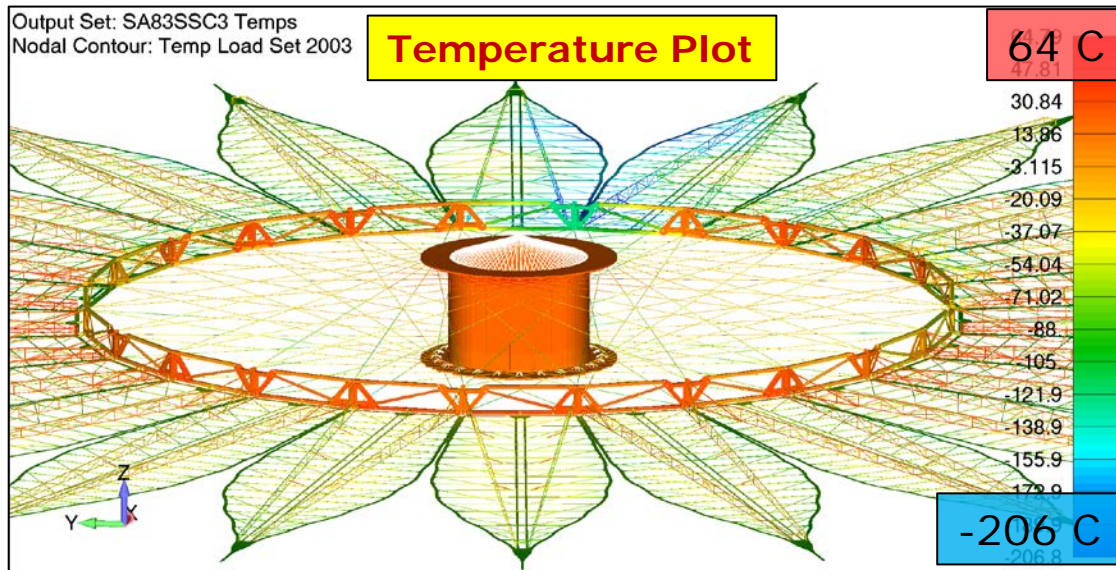
Sun Angle 83, NON-spinning, Distortions

- Sun Angle 83 degrees produces representative distortions and worst case contrast, shown as example of NON-spinning results
- **Raw** distortions on order of 75 microns (0.003")
- Distortions correspond to temperature results (thermal analysis), e.g.
 - Truss HOT @ 70 C (dT = 50C), ~25 micron radial expansion
- Cold Petals are longer, disrupts apodization function



Radial Translation

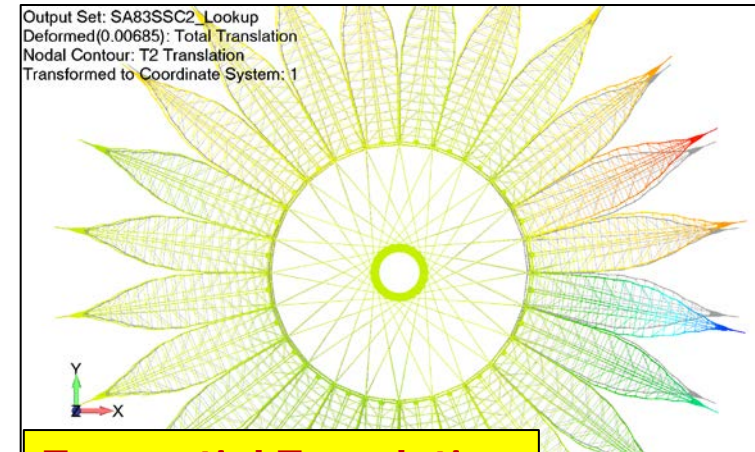
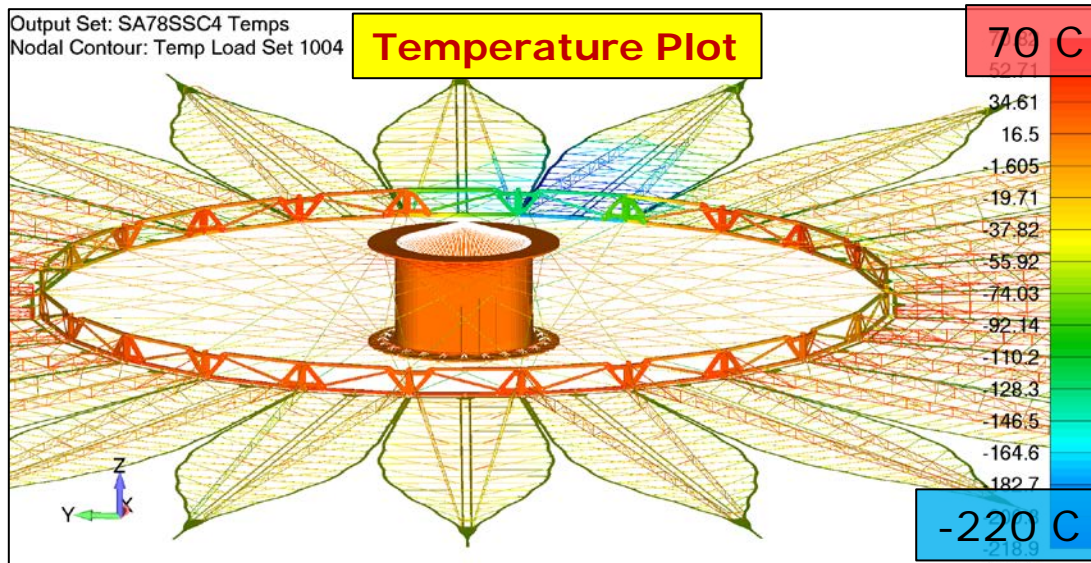
.0028"



.0001"

Sun Angle 83, NON-spinning, Distortions

- Sun Angle 83 degrees produces representative distortions for the steady state sun angle cases and is the worst case contrast for steady state, shown as example of NON-spinning results
- **Raw** distortions on order of 100 microns (0.004")
 - Truss bays in shadow are cold, and grow (neg CTE), and splay petals apart from each other



Tangential Translation

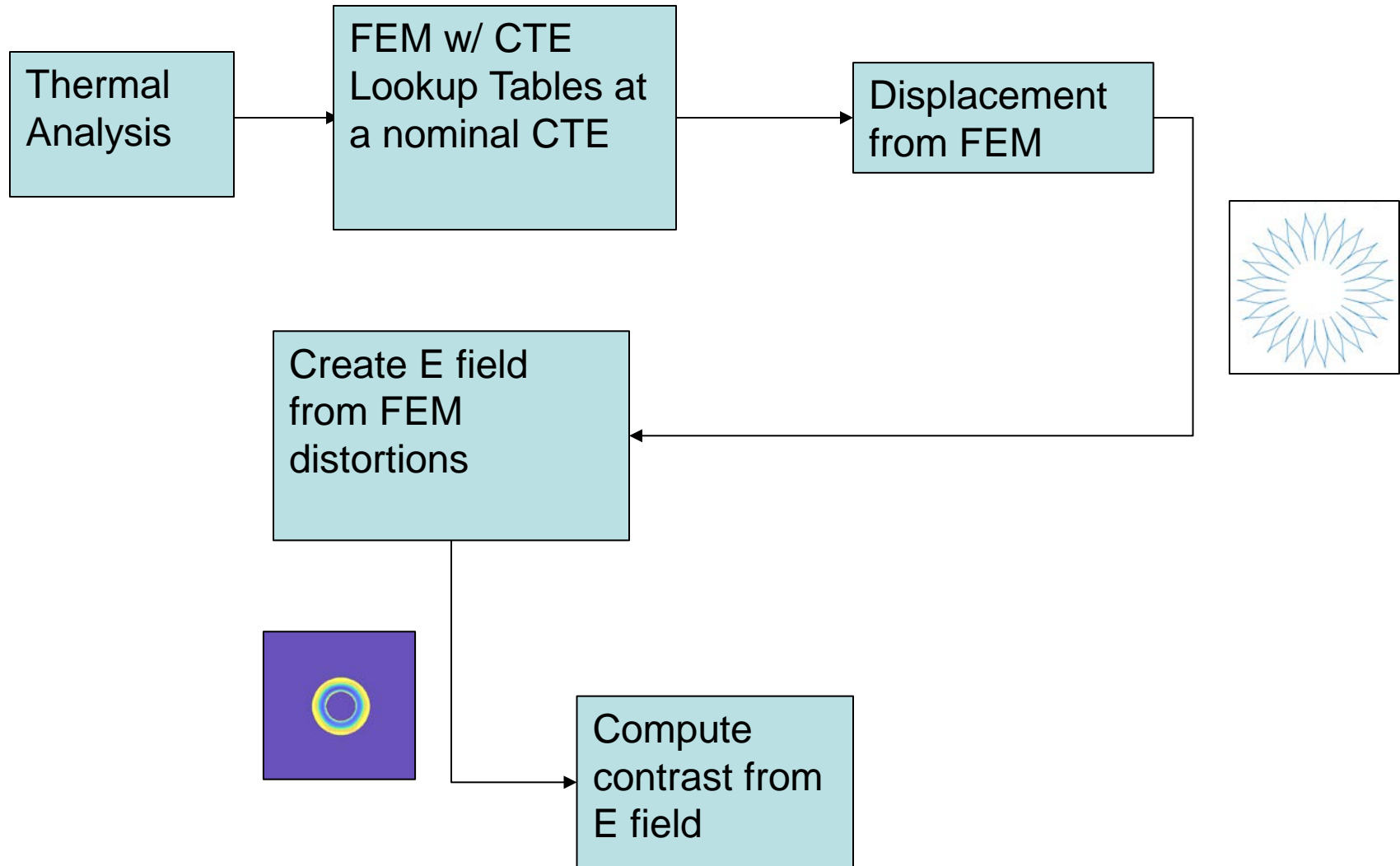
+ .0035"

-.0044"

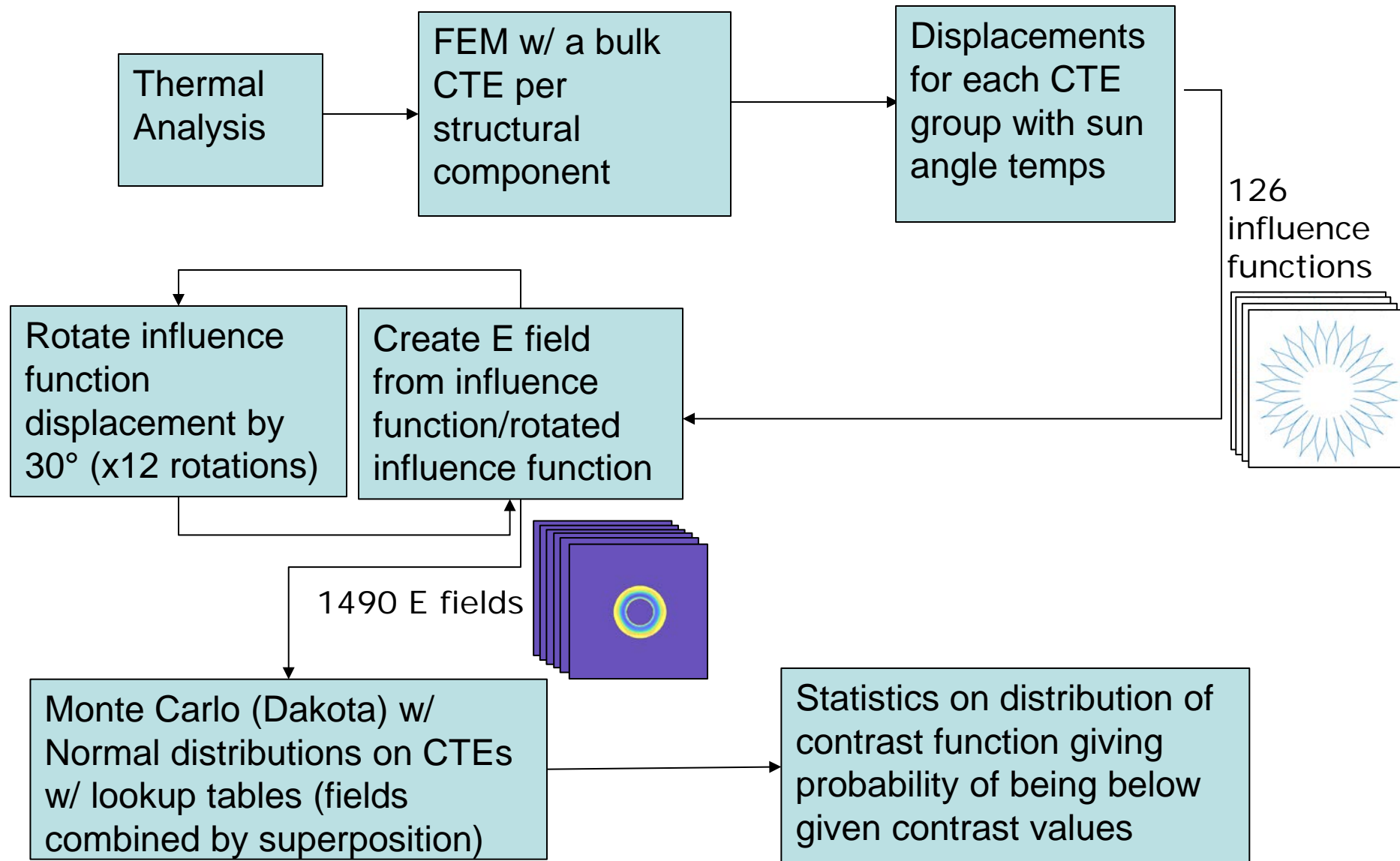
Thermal Distortion Analysis

- Two analyses for the impact of thermal distortion on contrast:
 - STOP Analysis: uses thermal mapping and nominal CTE values (temperature dependent) to compute contrast for each sun angle
 - Monte-Carlo Analysis: uses random distributions on CTEs to determine statistical distribution on contrast for each sun angle

STOP Analysis (for each sun angle)



Monte Carlo Analysis (for each sun angle)



Monte Carlo CTE Influence Functions

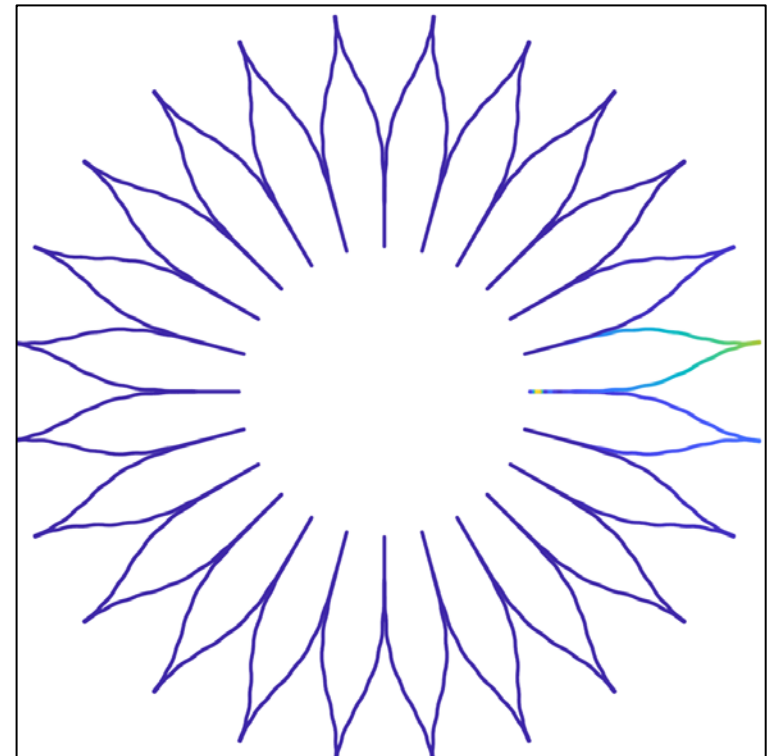
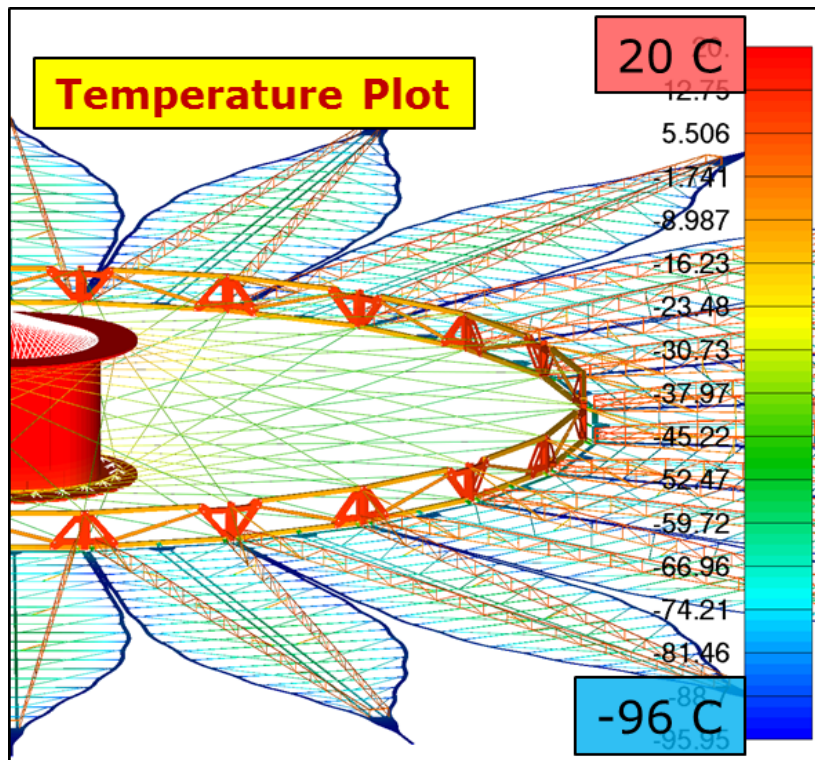
- Influence functions were created by setting a specified component at -1ppm/C CTE and all other components at 0 CTE with a given sun angle temperature mapping
- Assumed spinning Starshade

Component Group	Components Per Petal	Total Influence Functions per Petal Pair	Resulting E Fields (post rotations)
Battens	19	38	456
Braces	22	44	528
PUR	2	4	48
Spines	2	4	48
OE, OE TIP	3	6	72
Roots	1	2	24
Longerons	1	2	24
Shorterons	1	2	24
Diagonal	1	2	24
Nodes	2	4	48
Hinges	3	6	72
Struts	2	4	48
PUR Struts	2	4	48
Tip Structures	1	2	24
Spokes	N/A	1	1
Hub	N/A	1	1
		Total Number of Influence Functions = 126	Total Number of Computed E fields = 1490

Sample Case: Batten 1 on Petal 1, SA83

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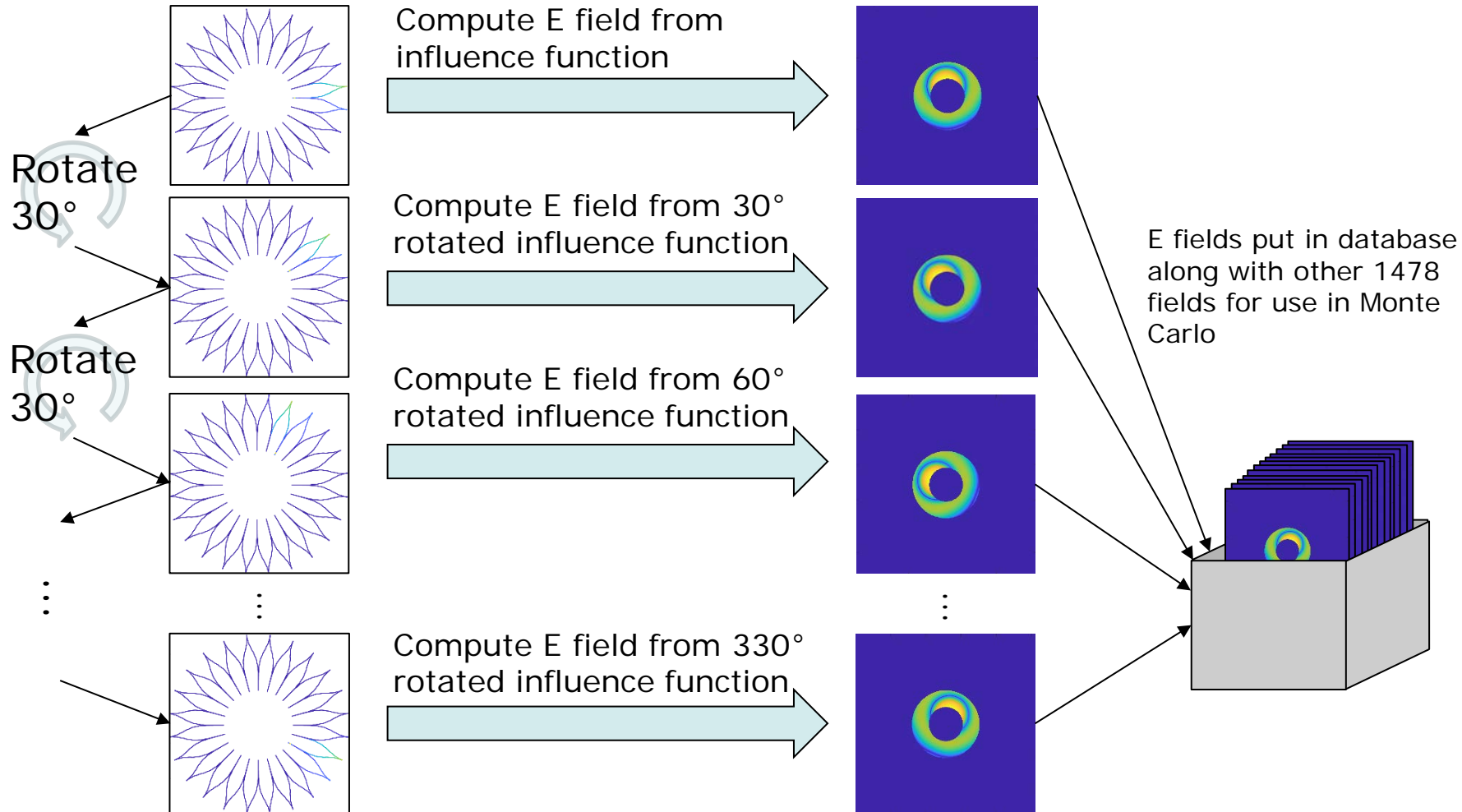
- FEM was run at SA83 with batten 1 on petal 1 at -1ppm/C CTE, everything else at 0 \rightarrow influence function (thermal distortion of perimeter)



Influence Function for batten 1
on petal 1, SA83

Sample Case: Batten 1 on Petal 1, SA83

- Compute the E field from the influence function, rotate 11 times and compute each E field:



Creating CTE Distributions w/ Lookup Tables

- 4 material lookup curves vs. temperature:
 - Intermediate modulus CFRP (petal battens and braces, spokes)
 - High Modulus CFRP (petal spine and root, truss longerons and nodes)
 - HM CFRP + AM foil (optical edge and tip)
 - Invar (petal hinges)
- Each lookup curve includes a nominal CTE with minimum and maximum error bands based on measured data
- Temperature statistics on each component group for a given spinning sun angle case:
 - Average temperature
 - Standard deviation
- Create CTE distributions assuming temperature is distributed between average temperature ± 3 std. dev.:
 - Average CTE = Nominal CTE @ average temperature
 - Average CTE + 1 std. dev. = Maximum CTE @ (average temp. + 3 std. dev.)
 - Average CTE - 1 std. dev. = Minimum CTE @ (average temp. - 3 std. dev.)

Creating CTE Distributions w/ Lookup Tables: Example

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- Sample case: SA83 batten 1 on petal 1
 - Material: IM CFRP
 - Average temperature: -73.4°C
 - Standard deviation: 4.2°C

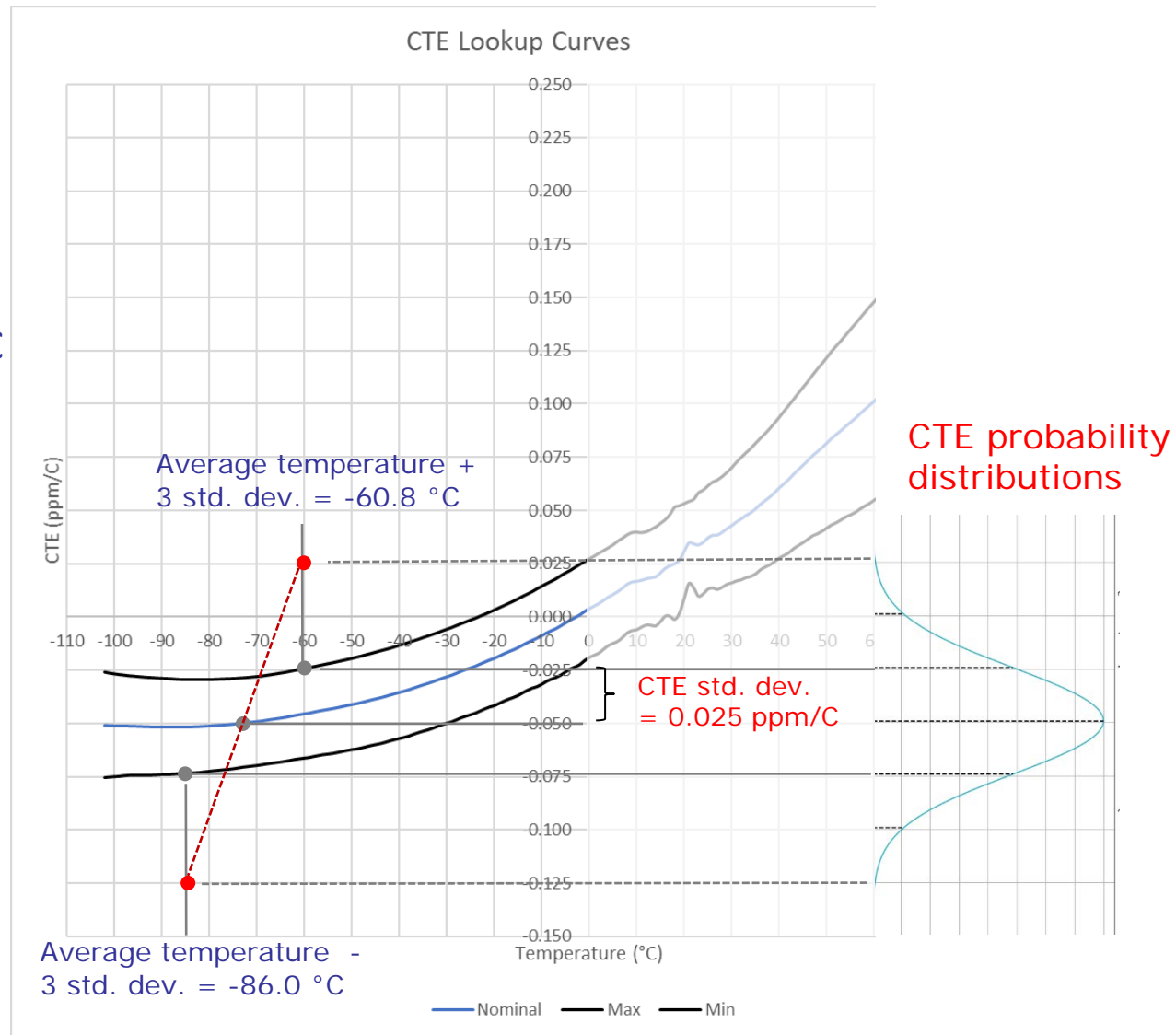
Normal Distribution Parameters:

Mean = -0.049 ppm/C

Std. Deviation =

upper bound – mean = 0.025 ppm/C

CTE 3σ range: $-.125$ to $+.025 \text{ ppm/C}$

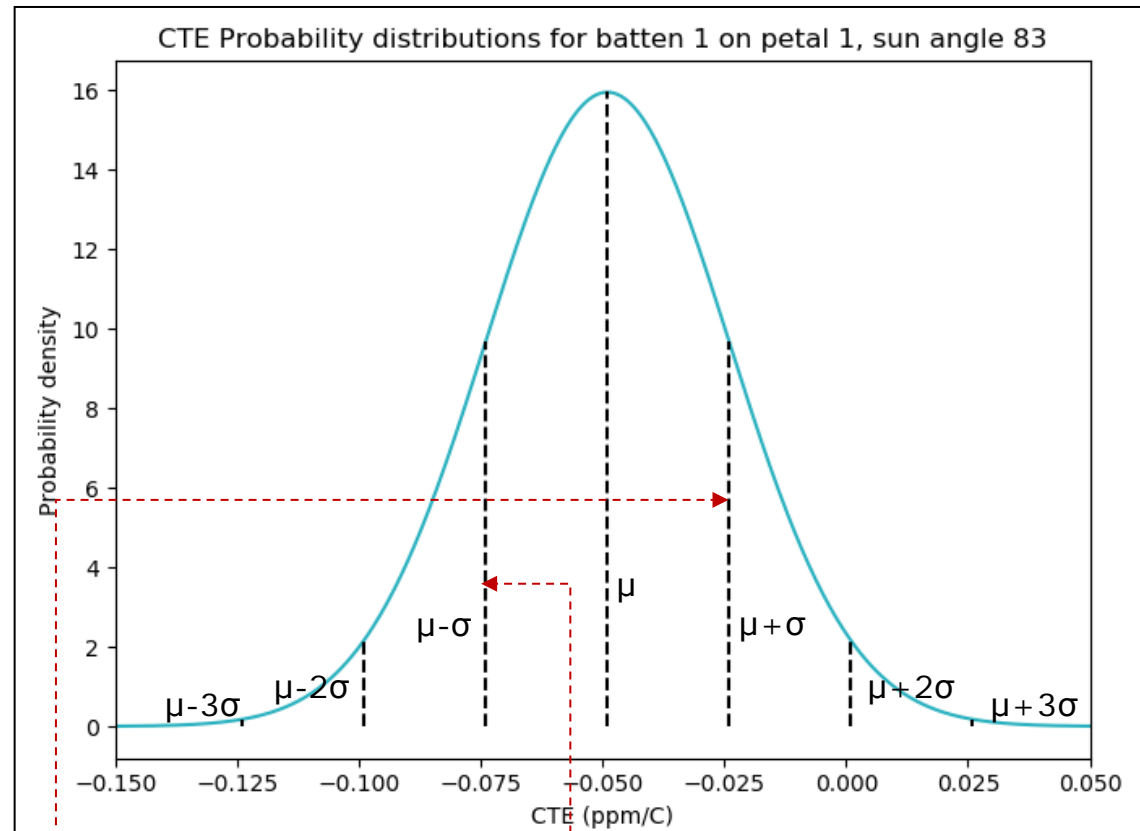
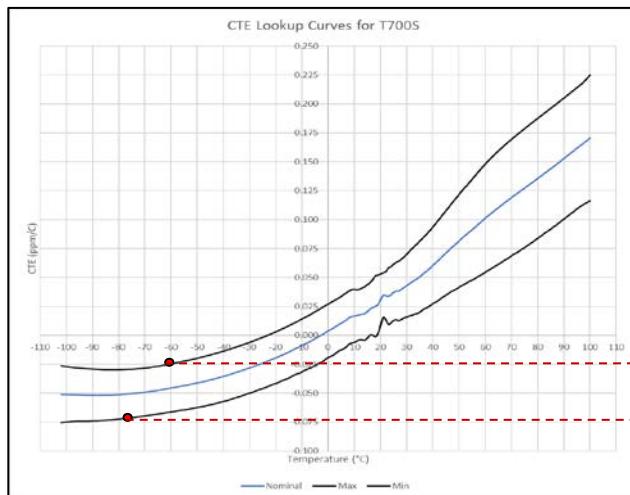


Creating CTE Distributions w/ Lookup Tables: Example

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CTE Distributions used in Monte Carlo analysis Sample case: SA83 batten 1 on petal 1

Normal Distribution Parameters:
Mean = -0.049 ppm/C
Std. Deviation = 0.025 ppm/C

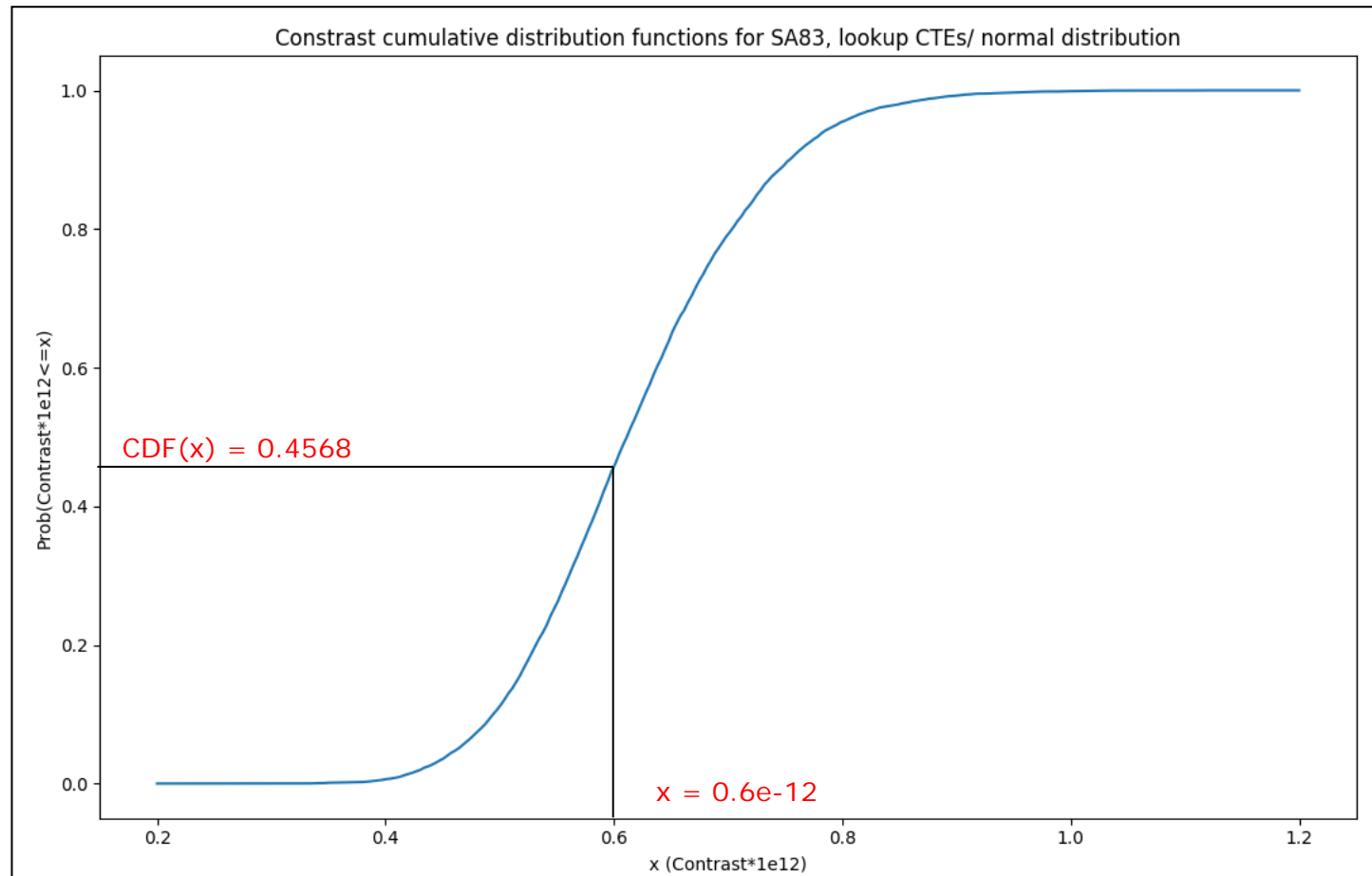


Statistical Results

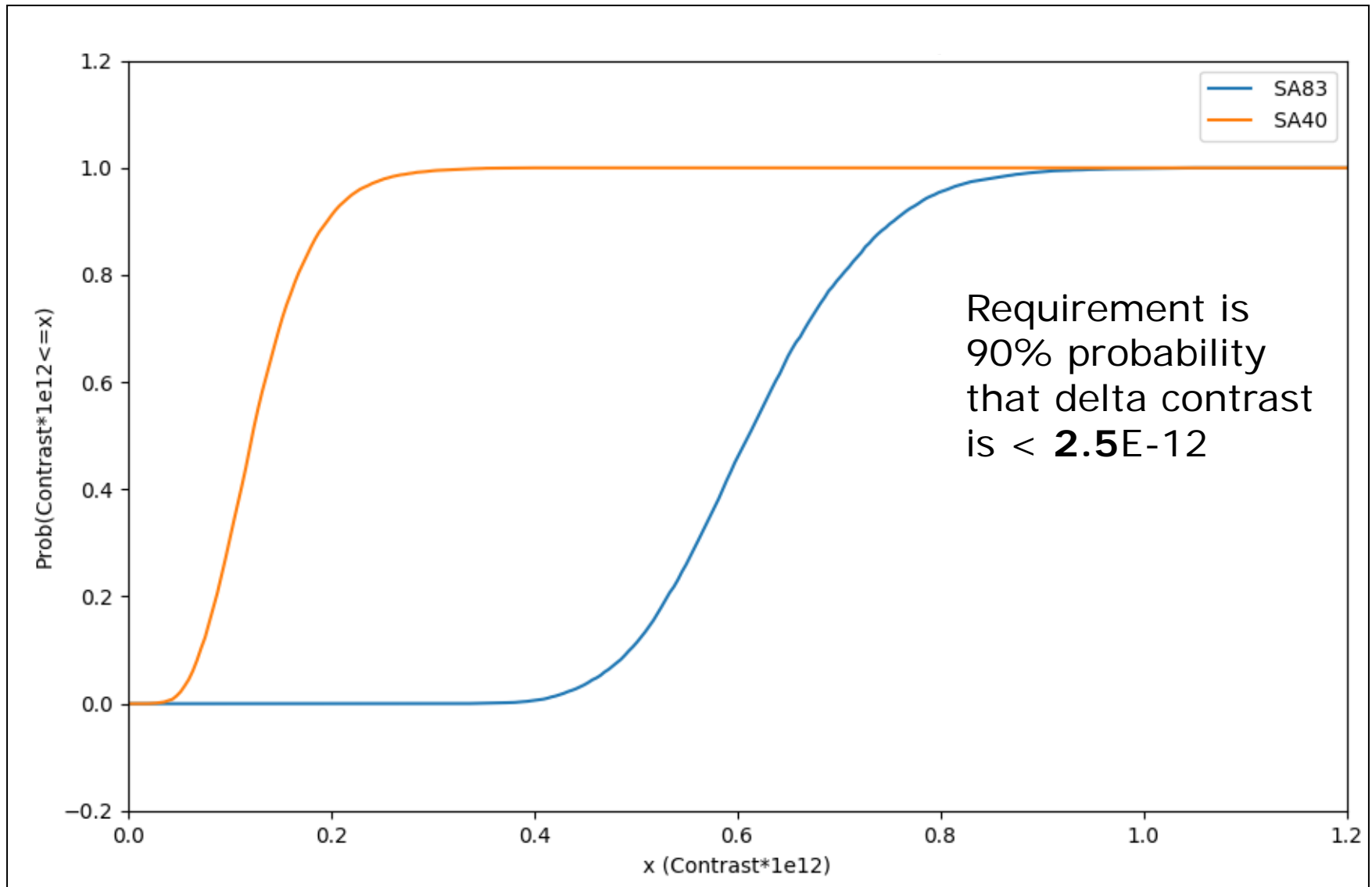
- From Monte-Carlo get:
 - Mean CTE and standard deviation w/ confidence intervals
 - Cumulative distribution function (CDF) for the contrast, which gives the probability that the contrast is below a given value (i.e. $\text{CDF}(x) = \text{Prob}(\text{contrast} \leq x)$)
 - Other statistical information, such as percentiles and correlations (which give information about which variables affect the contrast the most)

Cumulative Distribution Function Example

- Sun angle 83°, spinning
- Normal distribution on CTEs
- Probability that the contrast is below **0.6e-12** is 0.457



CDFs for all CTE Distributions and Sun Angles, Spinning



Results Summary - Spinning

Monte-Carlo Analysis Results:

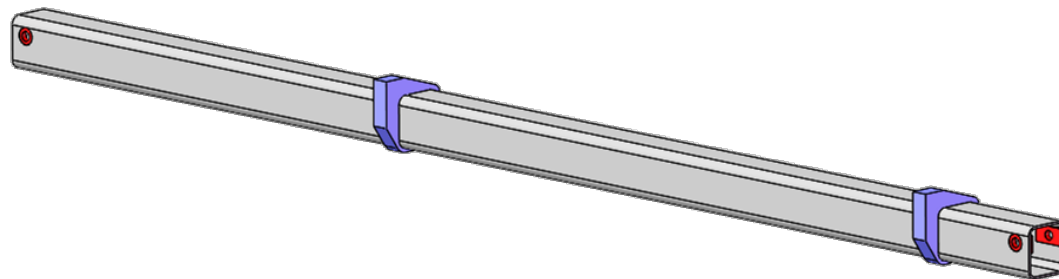
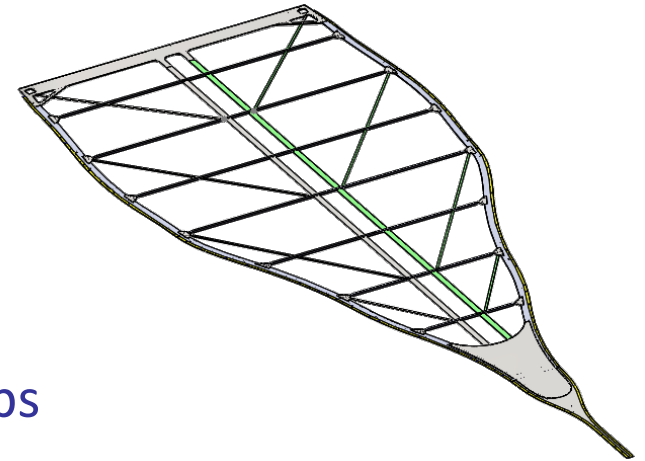
Sun Angle	Samples	Prob(contrast $\leq 2.5e-12$)	Mean contrast * $1e12$	90 th percentile * $1e12$
83°	10000	100%	0.619	0.754
40°	10000	100%	0.130	0.196

STOP Analysis Results:

Sun Angle	Contrast * $1e12$
83°	0.588
40°	0.025

Verification and Testing

- Fabricating a flight-like petal
 - High modulus CFRP QI layup for edge, root, spine and tip
 - Pultruded intermediate modulus carbon fiber/epoxy for battens and braces
 - Applying flight like bonding practices, fixturing and curing
- Fabricating a CTE truss bay
 - Longerons with bonded fittings
 - Node assembly with fittings and shear webs



Verification and Testing

- Testing

- Components' shape will be tested before and after thermal cycling
- Bonded assemblies will be shape tested before and after thermal cycling
- Raw components CTE tested (battens, braces, HM CFRP QI and Uni)
- Petal assemblies will be CTE tested (batten assembly)
- Petal will be tested in TVAC chamber with laser interferometry
- Truss longerons and nodes will be CTE tested

- Analysis Correlation

- Petal, longeron and node assemblies' finite element models will be checked against CTE results

